

On multicomponent two-phase flows with mass transfer

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International Workshop on Mathematical Fluid Dynamics

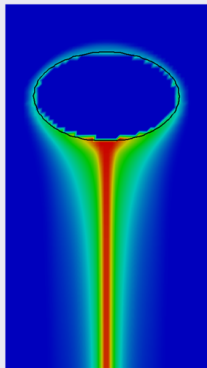
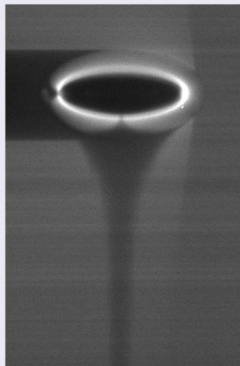
Waseda University, March 8-16, 2010

joint work with Jan Prüss

Motivation

Mass transfer from rising bubbles

Oxygen concentration around a rising air bubble



gas bubble:
 O_2 , N_2 , CO_2 ,
water vapor

ambient liquid:
water,
 O_2 , N_2 , CO_2

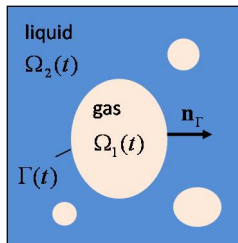
Sharp interface model

Continuum mechanical model with sharp interface

- captures the relevant macroscopic phenomena in many cases

Two-phase system

- continuous physical quantities inside the bulk phases
- jump discontinuities at the phase boundaries



Multicomponent system

- mixture of several chemical components
- partial miscibility

Multicomponent single-phase fluid mixture

chemical components A_1, \dots, A_n , possibly with chemical reactions

individual mass balances:

$$\partial_t \rho_i + \operatorname{div}(\rho_i \mathbf{u}_i) = M_i r_i^{\text{tot}} \quad \text{in } \Omega$$

$\rho_i = \rho_i(t, \mathbf{x})$ individual mass densities

$\mathbf{u}_i = \mathbf{u}_i(t, \mathbf{x})$ individual velocity fields

M_i molar mass of species i

r_i^{tot} molar rate of change due to chemical reactions

$\Omega \subset \mathbb{R}^n$ open domain with smooth boundary $\partial\Omega$

common variant: use molar concentrations $c_i := \rho_i / M_i$.

$$\partial_t c_i + \operatorname{div}(c_i \mathbf{u}_i) = r_i^{\text{tot}} \quad \text{in } \Omega$$

Multicomponent single-phase fluid mixture

assumption: isothermal conditions

individual momentum balances*:

$$\partial_t(\rho_i \mathbf{u}_i) + \nabla \cdot (\rho_i \mathbf{u}_i \otimes \mathbf{u}_i) = -c_i \nabla \mu_i + \nabla \cdot \mathbf{S}_i + \rho_i \mathbf{F}_i - c^{\text{tot}} R T \sum_{j \neq i} f_{ij} x_i x_j (\mathbf{u}_i - \mathbf{u}_j) \quad \text{in } \Omega$$

μ_i chemical potential of species i

\mathbf{S}_i viscous stress of species i

\mathbf{F}_i body forces acting on species i

c^{tot} sum of all molar concentrations

RT universal gas constant times absolute temperature

f_{ij} friction factor for collisions between species i, j ; $f_{ij} = f_{ji} > 0$

x_i molar fraction of species i ; $x_i = c_i / c^{\text{tot}}$

* P. Kerkhof, TU/e

Multicomponent single-phase fluid mixture

mixture balances

$$\rho := \sum_i \rho_i, \quad \rho \mathbf{u} := \sum_i \rho_i \mathbf{u}_i \quad (\Rightarrow \text{barycentric velocity } \mathbf{u})$$

continuity equation: (conservation of total mass, i.e. $\sum_i M_i r_i^{\text{tot}} = 0$)

$$\partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \quad \text{in } \Omega$$

individual mass balances:

$$\partial_t \rho_i + \operatorname{div}(\rho_i \mathbf{u} + \mathbf{j}_i) = M_i r_i^{\text{tot}} \quad \text{in } \Omega$$

with molecular fluxes $\mathbf{j}_i = \rho_i(\mathbf{u}_i - \mathbf{u})$ which need to be modeled.

Multicomponent single-phase fluid mixture

balance of total momentum:

for simplicity: no external forces

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = - \sum_i c_i \nabla \mu_i + \nabla \cdot \sum_i (\mathbf{S}_i + \frac{1}{\rho_i} \mathbf{j}_i \otimes \mathbf{j}_i)$$

Note: $\nabla_T \mu_i = \nabla_{T,p} \mu_i + v_i \nabla p$

with $v_i = \frac{\partial \mu_i}{\partial p}$ the partial molar volume, p the total pressure

Gibbs-Duhem: $\sum_i c_i \nabla_T \mu_i = \nabla p$

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = -\nabla p + \nabla \cdot \mathbf{S}$$

with the mixture stress tensor $\mathbf{S} = \sum_i (\mathbf{S}_i + \frac{1}{\rho_i} \mathbf{j}_i \otimes \mathbf{j}_i)$

Multicomponent single-phase fluid mixture

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Multicomponent single-phase fluid mixture

Class I mixture model (single-phase):

$$\text{total mass} \quad \partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0$$

$$\text{momentum} \quad \partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = -\nabla p + \nabla \cdot \mathbf{S}$$

$$\text{species mass} \quad \rho(\partial_t y_i + \mathbf{u} \cdot \nabla y_i) + \operatorname{div} \mathbf{j}_i = 0$$

with mass fractions $y_i = \rho_i / \rho$

Constitutive equations for multicomponent diffusive fluxes ?

Multicomponent single-phase fluid mixture

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Constitutive equations for multicomponent diffusive fluxes ?

Multicomponent single-phase fluid mixture

individual momentum balances in dimensionless form:

$$\begin{aligned} \partial_t(\rho_i^* \mathbf{u}_i^*) + \nabla \cdot (\rho_i^* \mathbf{u}_i^* \otimes \mathbf{u}_i^*) = & -\text{Eu} \phi_i \nabla p^* + \frac{1}{\text{Re}} \nabla \cdot \mathbf{S}_i^* \\ & - \text{MS} c_{\text{tot}}^* \left(x_i \nabla_{T,p} \mu_i^* + \text{Pe} \sum_{j \neq i} \frac{x_i x_j}{\mathfrak{D}_{ij}^*} (\mathbf{u}_i^* - \mathbf{u}_j^*) \right) \end{aligned}$$

with $\mathfrak{D}_{ij}^* = \mathfrak{D}_{ij}/\mathfrak{D}_0$, $\mathfrak{D}_{ij} = 1/f_{ij}$ the *Maxwell-Stefan diffusivities* and ϕ_i the volume fractions.

$$\begin{aligned} \text{Eu} = \frac{\rho_0}{\rho_0 U^2} \quad (\text{Euler number}), & \quad \text{Re} = \frac{\rho_0 U L}{\eta_0} \quad (\text{Reynolds number}) \\ \text{Pe} = \frac{U L}{\mathfrak{D}_0} \quad (\text{Péclet number}), & \quad \text{MS} = \frac{c_0 R T}{\rho_0 U^2} \end{aligned}$$

typical in applications: $\text{MS} \approx 10^5$

Multicomponent single-phase fluid mixture

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Multicomponent single-phase fluid mixture

requires, in the limit as $MS \rightarrow \infty$:

$$\left(x_i \nabla_{T,p} \mu_i^* + \text{Pe} \sum_{j \neq i} \frac{x_i x_j}{\mathfrak{D}_{ij}^*} (\mathbf{u}_i^* - \mathbf{u}_j^*) \right) = 0,$$

or, translated back to dimensional quantities:

$$\frac{x_i}{RT} \nabla_{T,p} \mu_i + \sum_{j \neq i} \frac{x_i x_j}{\mathfrak{D}_{ij}} (\mathbf{u}_i - \mathbf{u}_j) = 0$$

But pressure diffusion may not be negligible: $\frac{Eu}{MS} \not\approx 0!$
 ($Eu \approx 100$ for atmospheric pressure)

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Note: $-\nabla p$ accelerates the full mixture!

$-\frac{\nabla p}{\rho}$ force per mass, hence $-y_i \nabla p$ is the part of the total pressure leading to the acceleration of species i as part of the full mixture.

Multicomponent single-phase fluid mixture

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Multicomponent single-phase fluid mixture

single-phase fluid mixture with Maxwell-Stefan diffusion:

total mass $\partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0$

momentum $\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = -\nabla p + \nabla \cdot \mathbf{S}$

species mass $\rho(\partial_t y_i + \mathbf{u} \cdot \nabla y_i) + \operatorname{div} \mathbf{j}_i = 0$

diffusive fluxes $\hat{\mathbf{d}}_i = -\sum_{j \neq i} \frac{y_j \mathbf{j}_i - y_i \mathbf{j}_j}{\rho \hat{\mathcal{D}}_{ij}}, \quad \sum_i \mathbf{j}_i = 0$

mass based notations: $\hat{\mathbf{d}}_i = \frac{y_i}{RT} (\nabla_T \hat{\mu}_i - \frac{\nabla p}{\rho})$ with $\hat{\mu}_i = \mu_i / M_i$,

$$\hat{\mathcal{D}}_{ij} = M_i M_j \mathcal{D}_{ij}$$

Multicomponent two-phase fluid mixtures

chemical components A_1, \dots, A_n , partially miscible, no adsorption

individual mass balances:

$$\partial_t \rho_i + \operatorname{div}(\rho_i \mathbf{u}_i) = R_i \quad \text{in } \Omega \setminus \Gamma, \quad \llbracket \rho_i(\mathbf{u}_i - \mathbf{u}_\Gamma) \rrbracket \mathbf{n}_\Gamma = 0 \quad \text{on } \Gamma$$

$$\rho := \sum_i \rho_i, \quad \rho \mathbf{u} := \sum_i \rho_i \mathbf{u}_i, \quad \mathbf{j} = \rho(\mathbf{u} - \mathbf{u}_\Gamma) \cdot \mathbf{n}_\Gamma; \quad \sum_i R_i = 0$$

Continuity equation:

$$\partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0 \quad \text{in } \Omega \setminus \Gamma, \quad \llbracket \mathbf{j} \rrbracket = 0 \quad \text{on } \Gamma$$

Species equations:

$$\begin{aligned} \rho(\partial_t y_i + \mathbf{u} \cdot \nabla y_i) + \operatorname{div} \mathbf{J}_i &= 0 \quad \text{in } \Omega \setminus \Gamma, \\ \llbracket y_i \rrbracket j + \llbracket \mathbf{J}_i \rrbracket \mathbf{n}_\Gamma &= 0 \quad \text{on } \Gamma \end{aligned}$$

Multicomponent two-phase fluid mixtures

isothermal two-phase balances:

bulk

$$\partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0$$

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = -\nabla p + \nabla \cdot \mathbf{S}$$

$$\rho(\partial_t y_i + \mathbf{u} \cdot \nabla y_i) + \operatorname{div} \mathbf{j}_i = 0$$

interface

$$[[\mathbf{u}]] = [[\frac{1}{\rho}]] j \mathbf{n}_\Gamma$$

$$[[\mathbf{u}]] j - [[\mathbf{T}]] \cdot \mathbf{n}_\Gamma = \sigma \kappa \mathbf{n}_\Gamma$$

$$V_\Gamma = \mathbf{u} \cdot \mathbf{n}_\Gamma + j/\rho$$

$$[[y_i]] j + [[\mathbf{j}_i]] \mathbf{n}_\Gamma = 0$$

One more constitutive relation at the interface is missing!

Energy dissipation (isothermal case)

total free energy:

$$E = \int_{\Omega} \rho \left(\frac{1}{2} |\mathbf{u}|^2 + \psi \right) dx + \int_{\Gamma} \sigma do$$

with $\rho\psi(\theta, \rho_1, \dots, \rho_n)$ the free (available) energy density.

Euler relation:

$$\rho\psi + p = \sum_i \hat{\mu}_i \rho_i \quad \text{with chemical potentials } \hat{\mu}_i = \partial_{\rho_i}(\rho\psi)$$

energy dissipation:

$$\begin{aligned} \partial_t E = & \int_{\Omega} \left(-\mathbf{S} : \nabla \mathbf{u} + p \operatorname{div} \mathbf{u} + \sum_i \nabla \hat{\mu}_i \cdot \mathbf{j}_i \right) dx \\ & + \int_{\Gamma} j \left(\left[\frac{1}{2\rho^2} \right] j^2 - [\mathbf{n}_{\Gamma} \cdot \mathbf{S} \mathbf{n}_{\Gamma} / \rho] \right) do + \int_{\Gamma} \sum_i [\hat{\mu}_i] j_i do \end{aligned}$$

with $j_i := \rho_i (\mathbf{u}_i - \mathbf{u}_{\Gamma}) \cdot \mathbf{n}_{\Gamma} = j y_i + \mathbf{j}_i \cdot \mathbf{n}_{\Gamma}$; note that $[[j_i]] = 0$.

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with $j_j := \rho_j (\mathbf{u}_j - \mathbf{u}_{\Gamma}) \cdot \mathbf{n}_{\Gamma} = j y_j + \mathbf{j}_j \cdot \mathbf{n}_{\Gamma}$; note that $\llbracket j_j \rrbracket = 0$.

Chemical interface conditions

assumption: no interfacial energy dissipation

$$\left(\left[\left[\frac{1}{2\rho^2}\right]\right]j^2 - \left[\mathbf{n}_\Gamma \cdot \mathbf{S}\mathbf{n}_\Gamma/\rho\right] + \left[\hat{\mu}_1\right]\right)j + \sum_{i \neq 1} \left[\hat{\mu}_i - \hat{\mu}_1\right]j_i = 0$$

chemical interface conditions:

$$\left[\hat{\mu}_i\right] = \left[\mathbf{n}_\Gamma \cdot \mathbf{S}\mathbf{n}_\Gamma/\rho\right] - \left[\left[\frac{1}{2\rho^2}\right]\right]j^2 \quad \text{for all } i$$

note:

- the standard assumption in literature is $\left[\hat{\mu}_i\right] = 0$ for all i
- consistency with the second law also requires $\mathbf{S} : \nabla \mathbf{u} \geq 0$ and $\sum_i \nabla \hat{\mu}_i \cdot \mathbf{j}_i \leq 0$

related models: D. Bedeaux, Advance in Chemical Physics LXIV (1986),
W. Dreyer, WIAS preprint No. 869 (2003).

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chemical interface conditions:

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Multicomponent two-phase Navier-Stokes system

the full model:

bulk

$$\partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0$$

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = \nabla \cdot \mathbf{T}$$

$$\rho(\partial_t y_i + \mathbf{u} \cdot \nabla y_i) + \operatorname{div} \mathbf{j}_i = 0$$

$$\hat{\mathbf{d}}_i = - \sum_{j \neq i} \frac{y_j \mathbf{j}_i - y_i \mathbf{j}_j}{\rho \hat{\mathbf{D}}_{ij}}, \quad \sum_i \mathbf{j}_i = 0$$

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$$[[\mathbf{u}]] = [[\frac{1}{\rho}]] j \mathbf{n}_\Gamma$$

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$$V_\Gamma = \mathbf{u} \cdot \mathbf{n}_\Gamma + j/\rho$$

$$[[y_i]]_j + [[\mathbf{j}_i]] \mathbf{n}_\Gamma = 0$$

$$[[\hat{\mu}_i]] = [[\mathbf{n}_\Gamma \cdot \mathbf{S} \mathbf{n}_\Gamma / \rho]] - [[\frac{1}{2\rho^2}]] j^2$$

Note: an incompressible version with $\rho_\pm \equiv \text{const}_\pm$ is also consistent.

The Fluxes

Inversion of the MS-equations on $E = \{u \in \mathbb{R}^n : \sum_i u_i = 0\}$:

$$[\mathbf{J}_i] = X^{\frac{1}{2}} (A_{S|E})^{-1} X^{-\frac{1}{2}} [\mathbf{d}_i] = \frac{1}{RT} X^{\frac{1}{2}} (A_{S|E})^{-1} X^{\frac{1}{2}} [\nabla \mu_i].$$

Here $A_S := X^{-\frac{1}{2}} A X^{\frac{1}{2}}$ with $X = \text{diag}(x_1, \dots, x_n)$ and

$$A = \begin{bmatrix} -s_1 & & & d_{ij} \\ & \cdot & \cdot & \\ & d_{ij} & & -s_n \end{bmatrix}, \quad s_i = \sum_{k \neq i} \frac{x_k}{\mathfrak{D}_{ik}}, \quad d_{ij} = \frac{x_i}{\mathfrak{D}_{ij}}$$

is symmetric with $\sigma(A_{S|E}) \subset (-\infty, -\delta]$ for $\delta = \min\{1/\mathfrak{D}_{ij} : i \neq j\}$.

- $[\mathbf{J}_i] : [\nabla \mu_i] = \frac{1}{RT} \left((A_{S|E})^{-1} X^{\frac{1}{2}} [\nabla \mu_i] \right) : \left(X^{\frac{1}{2}} [\nabla \mu_i] \right) \leq 0$.
- $\text{div}([\mathbf{J}_i]) =: \text{div}(-\mathbf{D}(\mathbf{c})\nabla \mathbf{c})$ has elliptic principal part if $\rho\psi$ is strongly convex

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Isothermal isobaric single-phase case

Theorem

Let $\Omega \subset \mathbb{R}^N$ be open bounded with smooth $\partial\Omega$. Let $p > \frac{N+2}{2}$ and $\mathbf{c}_0 \in W_p^{2-\frac{2}{p}}(\Omega)$ such that $c_i^0 > 0$ in $\bar{\Omega}$ and c_0^{tot} is constant in Ω . Let the diffusion matrix $\mathbf{D}(\mathbf{c})$ be given by

$$\mathbf{D}(\mathbf{c}) = X^{\frac{1}{2}}(A_{S|E})^{-1}X^{\frac{1}{2}}G''(\mathbf{x}) \quad \text{with } \mathbf{x} = \mathbf{c}/c^{\text{tot}}, X = \text{diag}(\mathbf{x}),$$

where $G := \rho\psi$ is smooth and strongly convex on $\{c^{\text{tot}} = c_0^{\text{tot}}\}$. Then there exists - locally in time - a unique strong solution (in the L^p -sense) of

$$\partial_t \mathbf{c} + \text{div}(-\mathbf{D}(\mathbf{c})\nabla \mathbf{c}) = 0, \quad \partial_\nu \mathbf{c}|_{\partial\Omega} = 0, \quad \mathbf{c}|_{t=0} = \mathbf{c}_0$$

This solution is in fact classical.

Isothermal isobaric single-phase case

Idea of proof: Let u be given by $c_{\text{tot}} x_i = u_i + c_{\text{tot}}^0/n$.

- evolution for u lives in $E = \{u \in \mathbb{R}^n : \sum_i u_i = 0\}$
- $\text{div}(-\mathbf{D}(u)\nabla u) = \mathbf{D}(u)(-\Delta u) + \text{lower order terms}$
- $\lambda \in \mathbb{C}$ and $v \in E$ with $\mathbf{D}(u)v = \lambda v$ means

$$X^{\frac{1}{2}}(A_{S|E})^{-1}X^{\frac{1}{2}}G''(\mathbf{x})v = \lambda v.$$

$$\Rightarrow \langle (A_{S|E})^{-1}X^{\frac{1}{2}}G''(\mathbf{x})v, X^{\frac{1}{2}}G''(\mathbf{x})v \rangle = \lambda \langle v, G''(\mathbf{x})v \rangle.$$

- left-hand side > 0 and $\langle v, G''(\mathbf{x})v \rangle > 0$ by assumption on G , hence $\lambda > 0 \Rightarrow \sigma(\mathbf{D}(u)) \subset (0, \infty)$ in $\mathcal{L}(E; E)$.

Solutions stay non-negative because of the structure of diffusive fluxes:

$$\mathbf{J}_i(\mathbf{c}) = -D_i(\mathbf{c}) \text{grad } c_i + c_i \mathbf{F}_i(\mathbf{c}, \nabla \mathbf{c}).$$

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Idea of proof: Let u be given by $c_{\text{tot}} x_i = u_i + c_{\text{tot}}^0/n$.

- evolution for u lives in $E = \{u \in \mathbb{R}^n : \sum_i u_i = 0\}$
- $\operatorname{div}(-\mathbf{D}(u)\nabla u) = \mathbf{D}(u)(-\Delta u) + \text{lower order terms}$
- $\lambda \in \mathbb{C}$ and $v \in E$ with $\mathbf{D}(u)v = \lambda v$ means

$$\begin{aligned} X^{\frac{1}{2}}(A_{S|E})^{-1}X^{\frac{1}{2}}G''(\mathbf{x})v &= \lambda v. \\ \Rightarrow \langle (A_{S|E})^{-1}X^{\frac{1}{2}}G''(\mathbf{x})v, X^{\frac{1}{2}}G''(\mathbf{x})v \rangle &= \lambda \langle v, G''(\mathbf{x})v \rangle. \end{aligned}$$

- left-hand side > 0 and $\langle v, G''(\mathbf{x})v \rangle > 0$ by assumption on G , hence $\lambda > 0 \Rightarrow \sigma(\mathbf{D}(u)) \subset (0, \infty)$ in $\mathcal{L}(E; E)$.

Solutions stay non-negative because of the structure of diffusive fluxes:

$$\mathbf{J}_i(\mathbf{c}) = -D_i(\mathbf{c}) \operatorname{grad} c_i + c_i \mathbf{F}_i(\mathbf{c}, \nabla \mathbf{c}).$$

Multicomponent two-phase Navier-Stokes system

the full model:

bulk

$$\partial_t \rho + \operatorname{div}(\rho \mathbf{u}) = 0$$

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) = \nabla \cdot \mathbf{T}$$

$$\rho(\partial_t y_i + \mathbf{u} \cdot \nabla y_i) + \operatorname{div} \mathbf{j}_i = 0$$

$$\hat{\mathbf{d}}_i = - \sum_{j \neq i} \frac{y_j \mathbf{j}_i - y_i \mathbf{j}_j}{\rho \hat{\Delta}_{ij}}, \quad \sum_i \mathbf{j}_i = 0$$

interface

$$[[\mathbf{u}]] = [[\frac{1}{\rho}]] j \mathbf{n}_\Gamma$$

$$[[\mathbf{u}]] j - [[\mathbf{T}]] \cdot \mathbf{n}_\Gamma = \sigma \kappa \mathbf{n}_\Gamma$$

$$V_\Gamma = \mathbf{u} \cdot \mathbf{n}_\Gamma + j/\rho$$

$$[[y_i]] j + [[\mathbf{j}_i]] \mathbf{n}_\Gamma = 0$$

$$[[\hat{\mu}_i]] = [[\mathbf{n}_\Gamma \cdot \mathbf{S} \mathbf{n}_\Gamma / \rho]] - [[\frac{1}{2\rho^2}]] j^2$$

We focus on the incompressible version with constant total densities
 $\rho_\pm \equiv \text{const}_\pm$.

Two-Phase Navier-Stokes-Maxwell-Stefan system

work in progress

- in the case Γ is a graph over \mathbb{R}^{N-1} , the Lopatinski-Shapiro conditions are satisfied in the isobaric case.

Hence, in the isobaric case the associated linear system with planar interface has maximal L_p -regularity.

- next step: check whether the Maxwell-Stefan multicomponent diffusion system is normally elliptic in the non-isobaric case.

Volume of Fluid (VOF)-Method

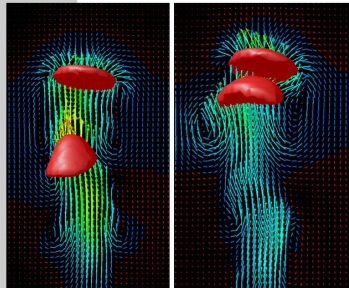
- Direct Numerical Simulation of Navier-Stokes equations for two-phase flows
- implicit representation of interface : volume tracking, fractional volume f of dispersed phase

- additional advection equation for f

$$\partial_t f + \mathbf{u} \cdot \nabla f = 0$$

- piecewise linear interface reconstruction
- surface tension: conservative model
- massively parallelized
- well validated for collision of drops

Rieber, Frohn, *ITLR Stuttgart*



0	0	0	0	0
0.87	0.52	0.08	0	0
1	1	0.53	0	0
1	1	0.95	0	0

VOF-based Mass-Transfer Computation

mass balance in terms of molar concentration c_i :

$$\partial_t c_i + \nabla \cdot c_i \mathbf{u} + \nabla \cdot \mathbf{J}_i = r_i \quad \left[[c_i(\mathbf{u} - \mathbf{u}_\Gamma) + \mathbf{J}_i] \right] \cdot \mathbf{n}_\Gamma = 0$$

- molecular fluxes according to Fick's law $\mathbf{J}_i^j = -D_i^j \nabla c_i^j, \quad j = L, G$
- no phase change: $\left[[c_i(\mathbf{u} - \mathbf{u}_\Gamma)] \right] \cdot \mathbf{n}_\Gamma = \mathbf{0}, \quad \mathbf{J}_i^L \cdot \mathbf{n}_\Gamma = \mathbf{J}_i^G \cdot \mathbf{n}_\Gamma$
- local chemical equilibrium: $\mu_i^G = \mu_i^L$

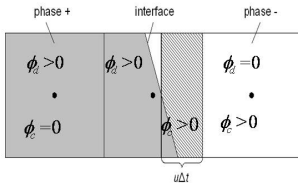
Henry's law: $\frac{c_i^G}{c_i^L} = H_i$

$$\mu_i = \mu_i^0 + RT \ln a_i \quad \begin{array}{l} a_i \text{ activity} \\ a_i = \gamma_i c_i \end{array}$$

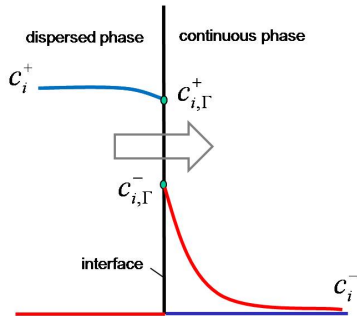
Two-Variable Mass-Transfer Approach

Problem: discontinuous species concentrations

- two scalar quantities per species
- convective transport interlinked with VOF-transport using geometrically computed fluxes

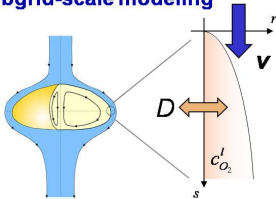


➡ no artificial mass transfer

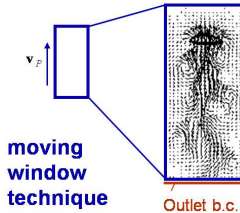
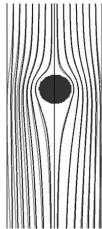


Enhancing the Interfacial Resolution

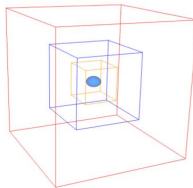
Subgrid-scale modeling



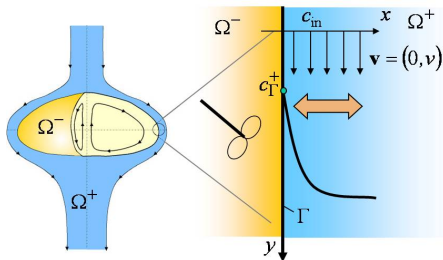
artificial
boundary
conditions
(ABCs)



Adaptive mesh refinement



Subgrid-Scale Modeling



$$\partial_t c + \mathbf{v} \cdot \nabla c = D \Delta c$$

$$t > 0, x > 0, y > 0$$

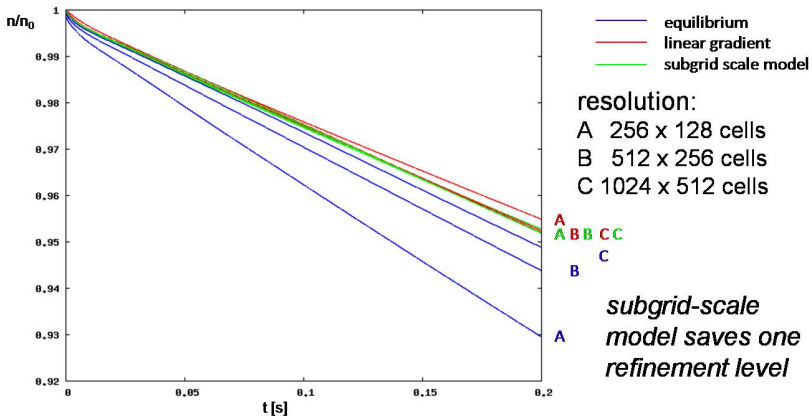
$$c|_{y=0} = c_{\text{in}}$$

$$c|_{x=0} = c_{\Gamma}^+$$

$$c|_{x=\infty} = 0$$

$$c(x, y) = c_{\Gamma}^+ \left(1 - \operatorname{erf} \left(\frac{x}{d(y)} \right) \right)$$

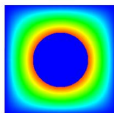
Effect of Subgrid-Scale Model



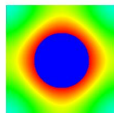
Evolution of species mass inside a rising 3 mm Blaise, 2D, $Sc = 10$

*subgrid-scale
model saves one
refinement level*

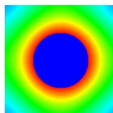
Artificial Boundary Condition



Dirichlet-BC



Neumann-BC



Robin-type BC

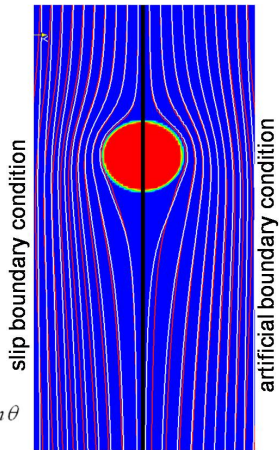
Hadamard-Rybczynski

$$u_r = \left(\frac{a_1}{r^3} + \frac{a_2}{r} - u_p \right) \cos \theta$$

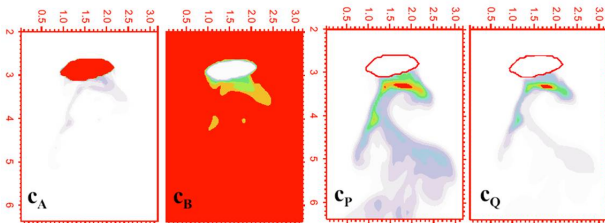
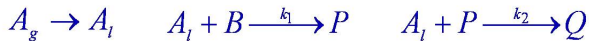
$$u_\theta = \left(\frac{1}{2} \frac{a_1}{r^3} - \frac{1}{2} \frac{a_2}{r} + u_p \right) \sin \theta$$

$$\frac{\partial u_r}{\partial r} + \frac{1}{r} u_r \approx -\frac{u_p}{r} \cos \theta$$

$$\frac{\partial u_\theta}{\partial r} + \frac{1}{r} u_\theta \approx \frac{u_p}{r} \sin \theta$$



Mass Transfer with Chemical Reaction



3D VOF-simulation

Acknowledgement

Many thanks to my co-workers:

- Andreas Alke
- Michael Kröger
- Dominik Weirich

Many thanks to the German Science Foundation (DFG):

- SPP 1141 *Mixing in Fluid Flows with and without Chemical Reactions*
- PAK 119 *Reactive Mass Transfer from Rising Gas Bubbles*

Many thanks to You for Your attention !