

Absorption of gas by a falling liquid film



TECHNISCHE
UNIVERSITÄT
DARMSTADT

Christoph Albert Dieter Bothe

Mathematical Modeling and Analysis

Center of Smart Interfaces/

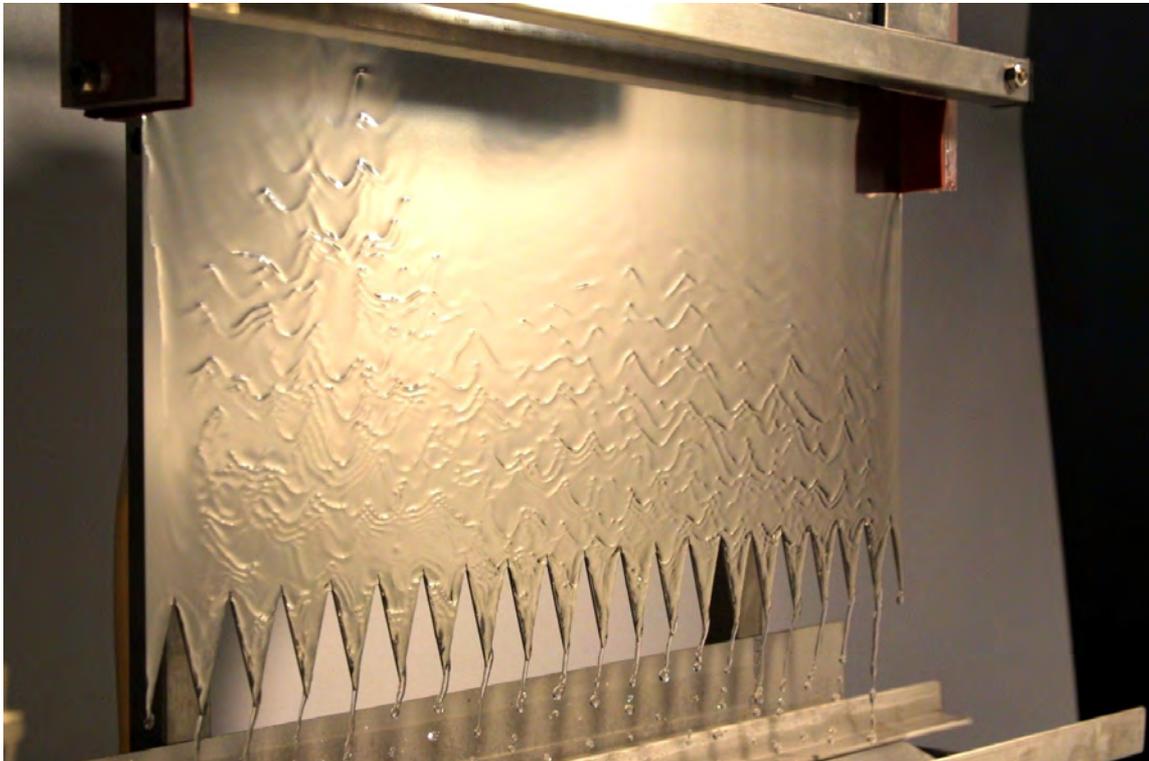
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Wavy Falling Films



- Advantages
 - Good heat transfer due to small thickness
 - Large Interface
- Applications
 - Evaporation
 - Cooling
 - Absorption

Assumptions

- Incompressible, Newtonian two-phase flow
- No phase transition
- Constant surface tension

$$\begin{aligned}\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla p &= \nabla \cdot \mathbf{S} + \rho \mathbf{g}, & \Omega \setminus \Sigma \\ \nabla \cdot \mathbf{u} &= 0, & \Omega \setminus \Sigma \\ \llbracket p \mathbf{I} - \mathbf{S} \rrbracket \cdot \mathbf{n}_\Sigma &= \sigma \kappa \mathbf{n}_\Sigma, & \Sigma \\ \llbracket \mathbf{u} \rrbracket &= 0, & \Sigma \\ \mathbf{S} &= \eta (\nabla \mathbf{u} + (\nabla \mathbf{u})^T)\end{aligned}$$

The Volume of Fluid Method

One Fluid Formulation:

$$\partial_t(\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla p = \nabla \cdot \mathbf{S} + \rho \mathbf{g} + \delta \mathbf{f}_\Sigma$$

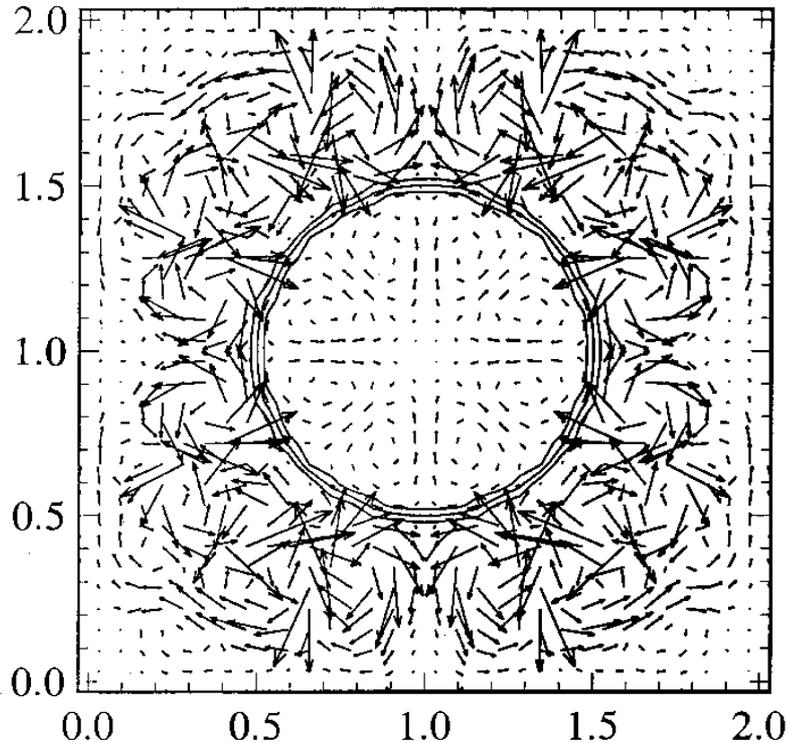
$$\nabla \cdot \mathbf{u} = 0$$

$$\partial_t f + \mathbf{u} \cdot \nabla f = 0$$

- Density and viscosity depend on volume fraction
- Volume fraction has to be transported
- Additional surface tension force term \mathbf{f}_Σ

0	0	0	0	0
0.87	0.52	0.08	0	0
1	1	0.53	0	0
1	1	0.95	0	0

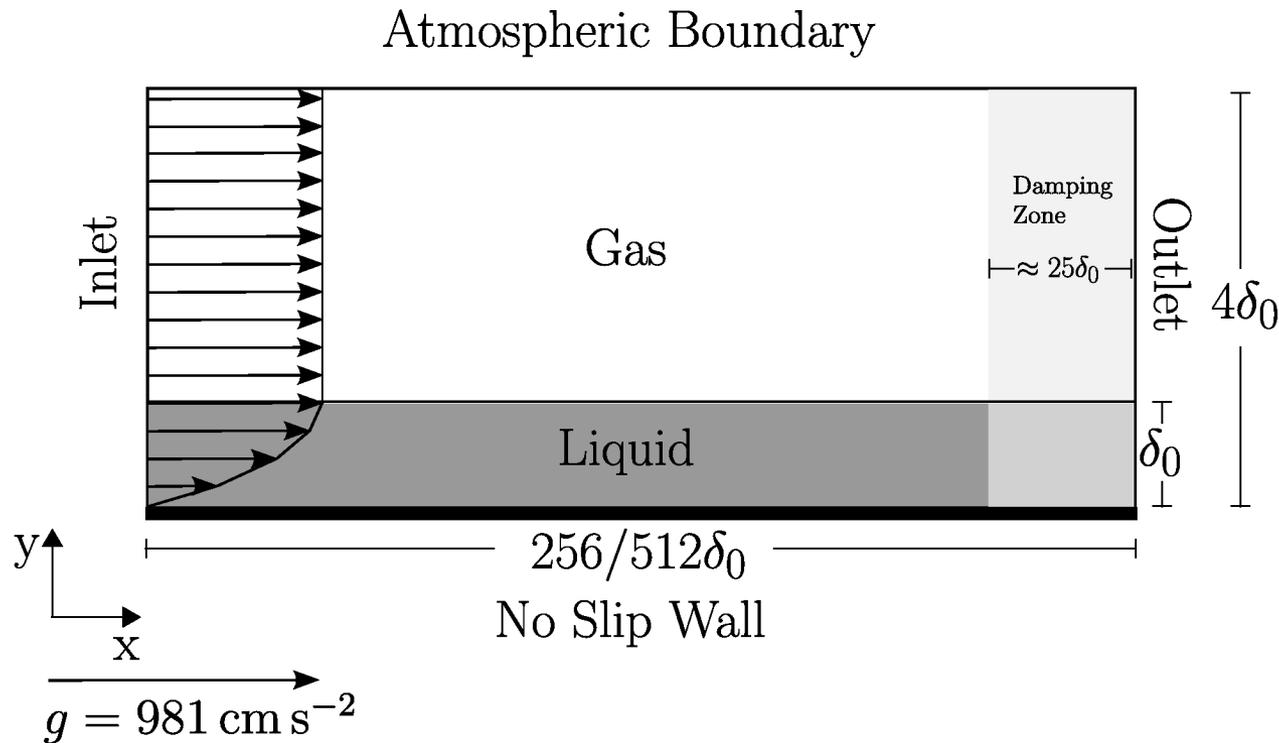
Parasitic Currents



Parasitic Currents in a VOF simulation
of a static droplet

- VOF simulations suffer from unphysical oscillation of velocity, so-called parasitic currents
- Stem from numerical treatment of interfacial jump condition for stress:
$$\llbracket p \mathbf{I} - \mathbf{S} \rrbracket \cdot \mathbf{n}_\Sigma = \sigma \kappa \mathbf{n}_\Sigma$$
- Especially serious in stagnant flow situations
- Also problematic in simulations of falling films, which are convection dominated

Numerical Setup



$$\mathbf{u}(t, y)|_{x=0} = \left(1 + \epsilon \sin(2\pi\omega t) \right) \left(\frac{\rho_l}{\mu_L} g \delta_0^2 \left[\frac{y}{\delta_0} - \frac{1}{2} \left(\frac{y}{\delta_0} \right)^2 \right], 0 \right)$$

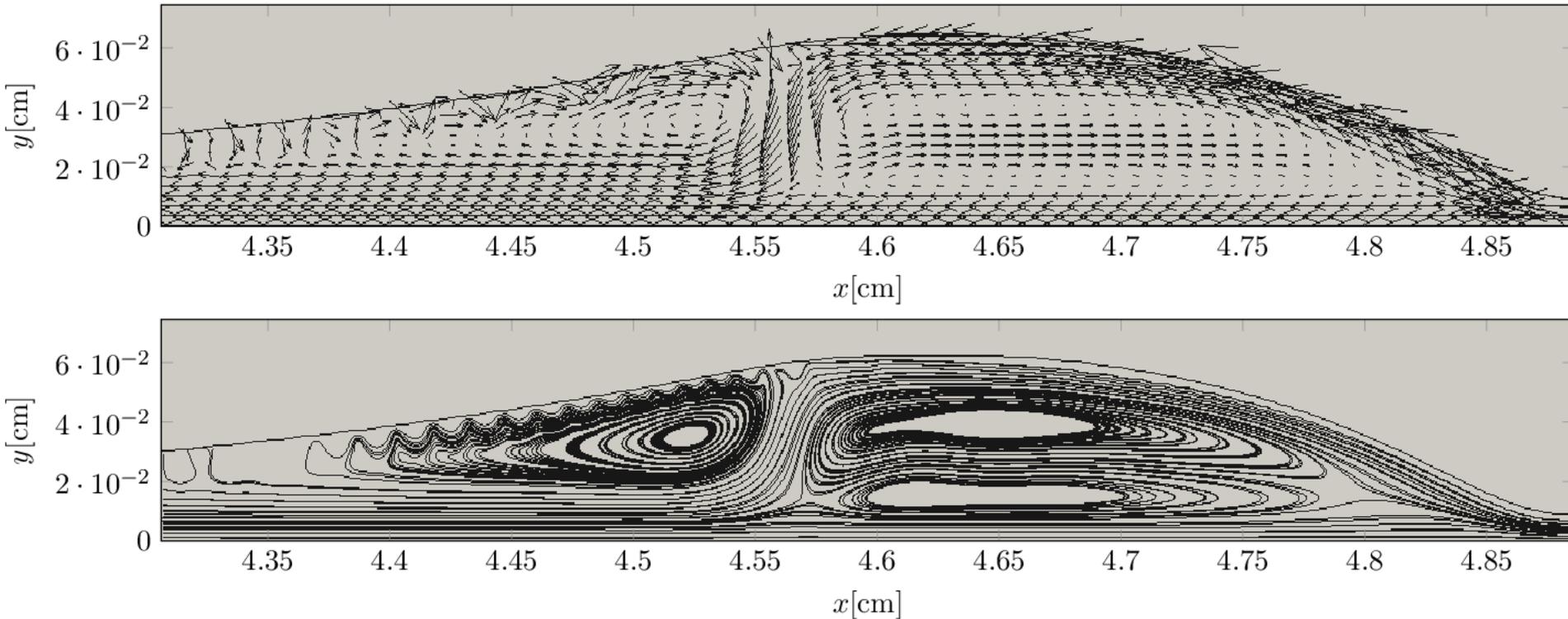
Continuum Surface Stress (CSS)



Body Force $\nabla \cdot (|\nabla f| \sigma (I - \vec{n}_\Sigma \otimes \vec{n}_\Sigma)),$

- Approximate \vec{n}_Σ by differentiating a smoothed f-field
- Momentum conservative
- Standard Surface Tension model in FS3D; delivers good results in many two-phase flow situations.

Falling Films with CSS



Water/Air, Re 60

- 16 cells per mean film thickness (0.265mm)
- $A = 30\%$, $f = 20$ Hz

Continuum Surface Force (CSF)

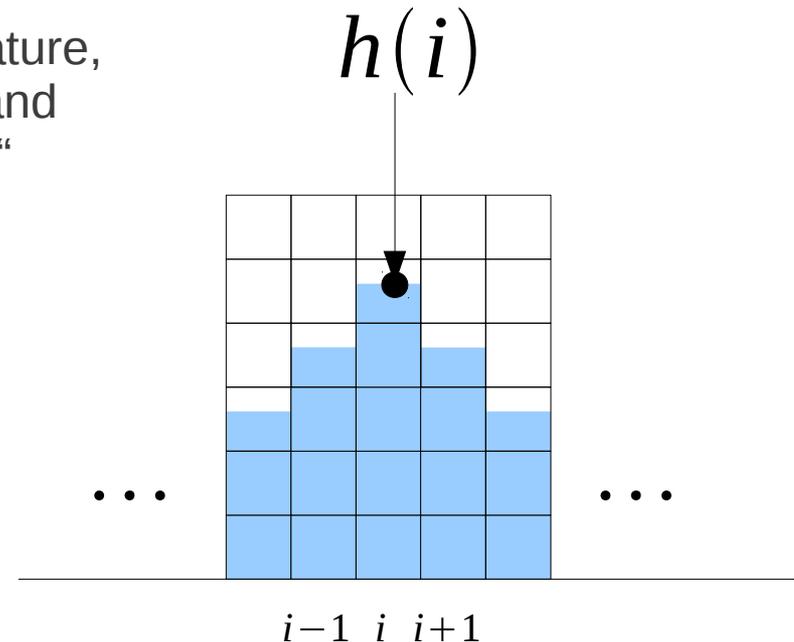
Body Force $\sigma \kappa \nabla f$

- In the case of a sphere and constant curvature, an exact balance between surface tension and pressure can be achieved: „Balanced Force“

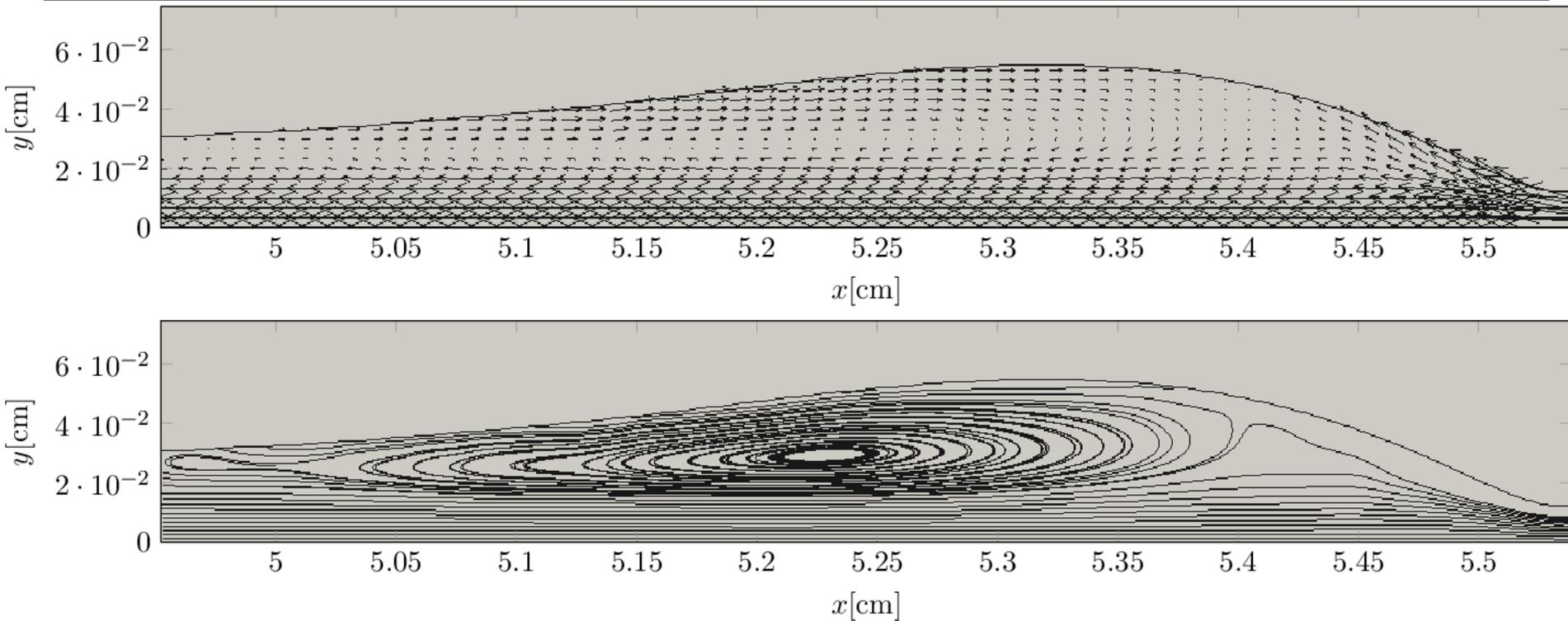
Renardy, J. *Comput. Phys.* 183 (2002)

- Greatly reduces parasitic currents
- Relies on „good“ curvature information

- Easy for a falling film: $\kappa = \frac{h_{xx}}{(1 + h_x^2)^{\frac{3}{2}}}$



Falling Films with CSF



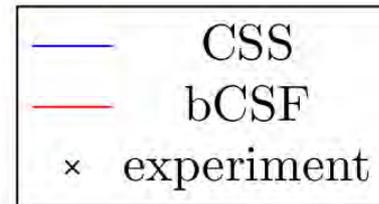
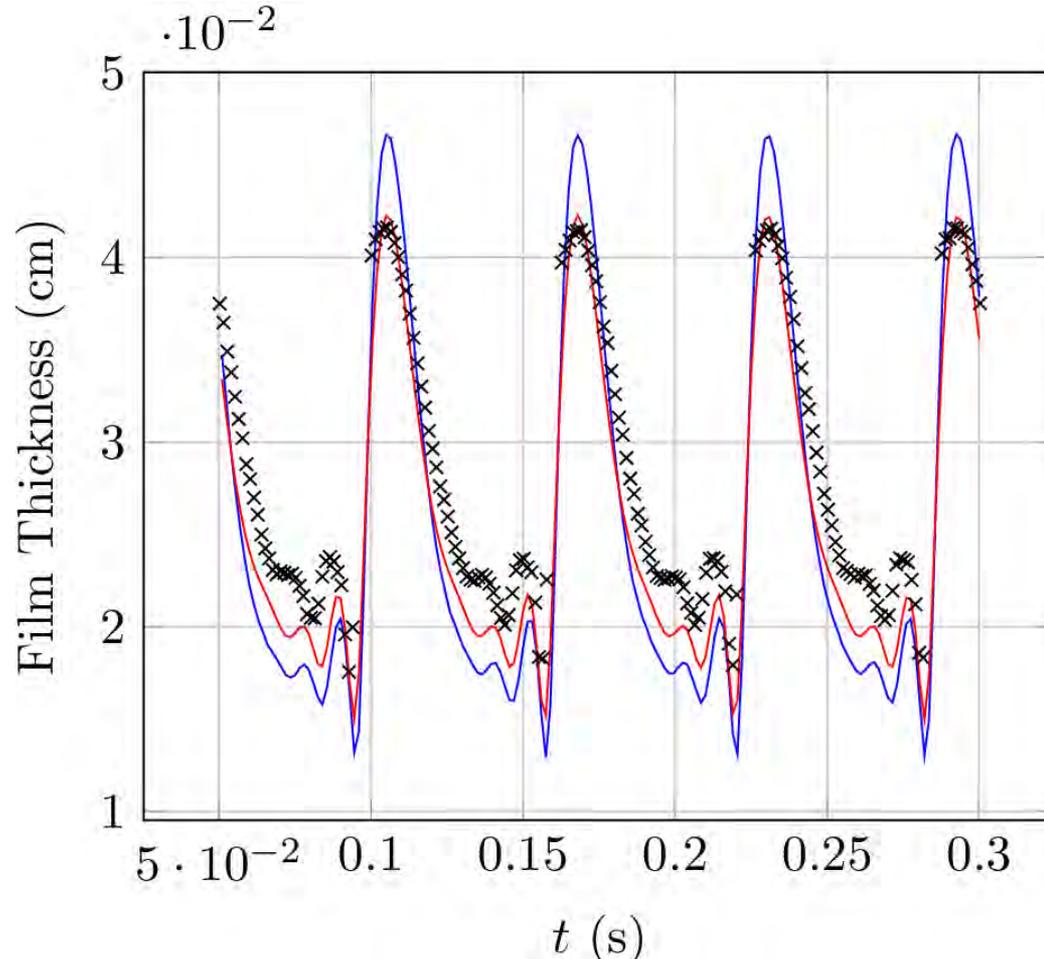
Water/Air, Re 60

- 16 cells per mean film thickness (0.265mm)
- $A = 30\%$, $f = 20$ Hz

Comparison to experiment: Dietze

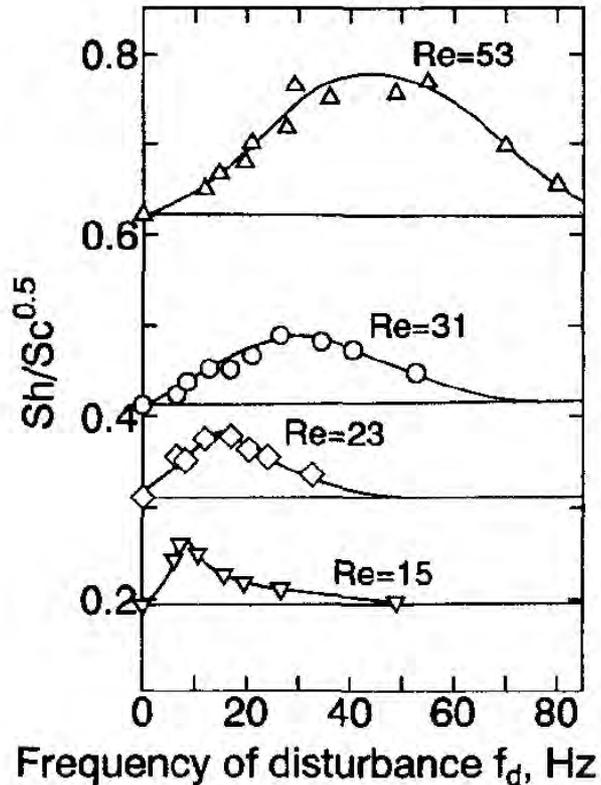
- Experimental data from **G.F. Dietze,
Flow Separation in Falling Liquid Films, 2010**
 - DMSO/Air
 - $\nu = 2.85 \cdot 10^{-6} \frac{m^2}{s}$, $\rho = 1098.3 \frac{kg}{m^3}$, $\sigma = 0.0484 \frac{N}{m}$
 - $Re = 8.6$
 - $f = 16$ Hz
 - $A = 40\%$
 - Resolution $\frac{\delta}{16}$

Comparison to experiment: Film thickness



- Film thickness at $x = 56$ mm over a time span of 0.3 s
- CSS overshoots

Species Transport in Falling Films



Data from Yoshimura et.al., 1996

Transport of Oxygen into a water film at 18°C

$$Sc = \frac{v_L}{D} = 570$$

$$Sh = \frac{k_L \delta_0}{D}$$

$$k_L = \frac{\Gamma}{L} \ln \left(\frac{C_S - C_{in}}{C_S - C_{out}} \right)$$

Species Transport in Falling Films: Model

Assumptions:

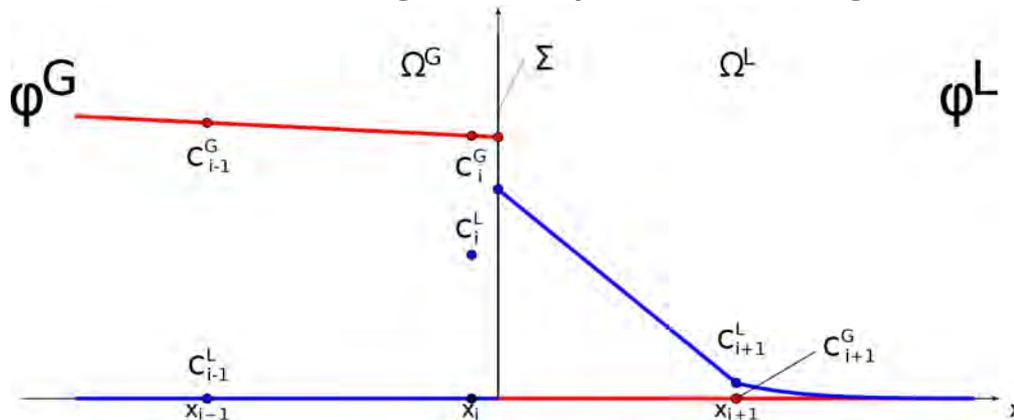
- Dilute system => species bears no mass or momentum, and does not affect viscosity
- No adsorption at the interface => surface tension stays constant
- No chemical reaction
- Local thermodynamic equilibrium at the interface => Henry's law holds
- Constant Henry coefficient

$$\begin{aligned}\partial_t c + \mathbf{u} \cdot \nabla c &= D \Delta c, & \Omega^G(t) \cup \Omega^L(t) \\ \llbracket -D \nabla c \rrbracket \cdot \mathbf{n}_\Sigma &= 0, & \Sigma \\ c_L &= H c_G, & \Sigma\end{aligned}$$

Numerical Approach

Two scalar approach with one-sided concentration gradient transfer flux

- Concentration is advected in the same way as volume fraction
- Two concentrations stored in each interfacial cell
- Both concentrations and Henry's law yield interfacial concentration
- Concentration gradient in liquid phase computed between interface and some value in bulk by subgrid model
- Diffuse flux from gas to liquid according to Fick's Law



$$\phi^G = c \chi_{\Omega^G}$$
$$\phi^L = c \chi_{\Omega^L}$$

Calculations

Water film at 18°C in
„Oxygen“ atmosphere

Resolution $\frac{\delta_0}{16}$

$Re = 31$

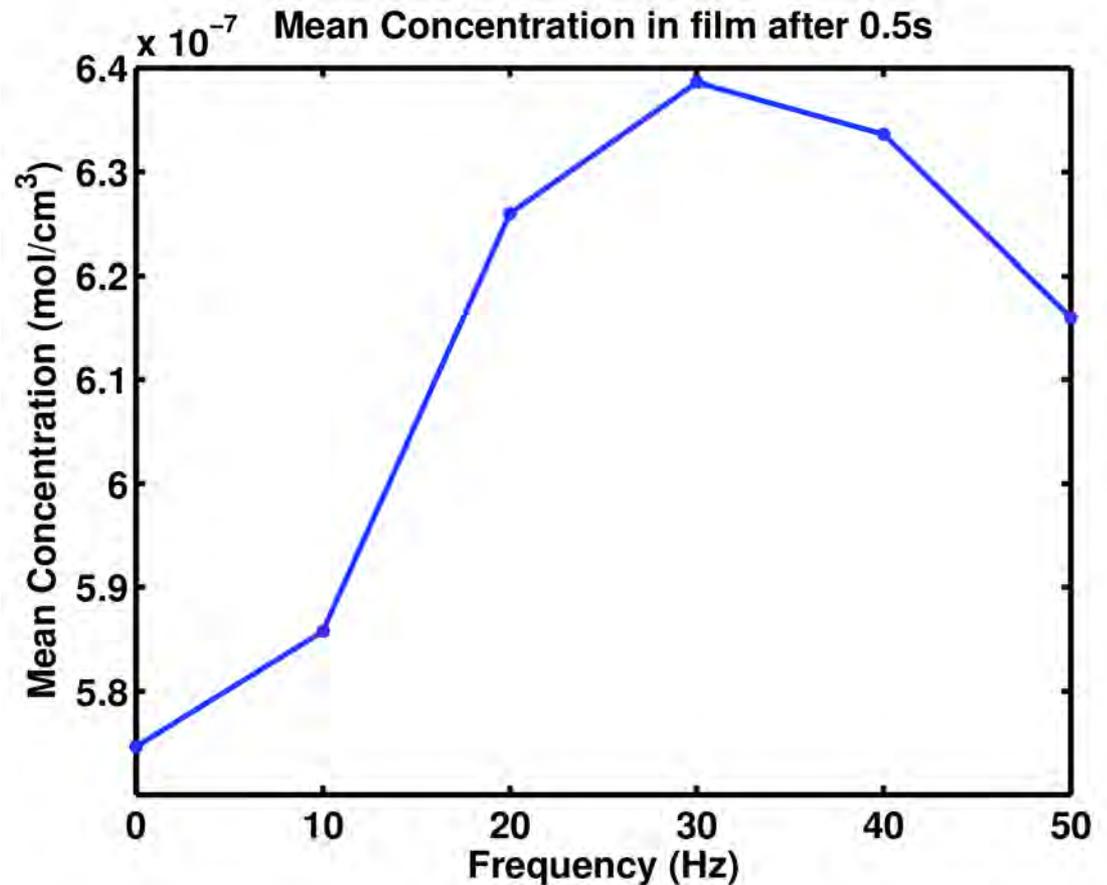
$Sc = 50$

$k_{H,cc} = 0.0270$

$c_G = 4.19e-5$

$c_{L,0} = 2.37e-7$

$D = 2.14e-4$



Validation: Method

Solve stationary advection diffusion
problem

on domain

with boundary conditions.

Solved with Matlab ODE Solver, by
defining x as pseudotime.

$$u(y)\partial_x c = D\partial_y^2 c$$

$$[0, x_{max}] \times [0, \delta_0]$$

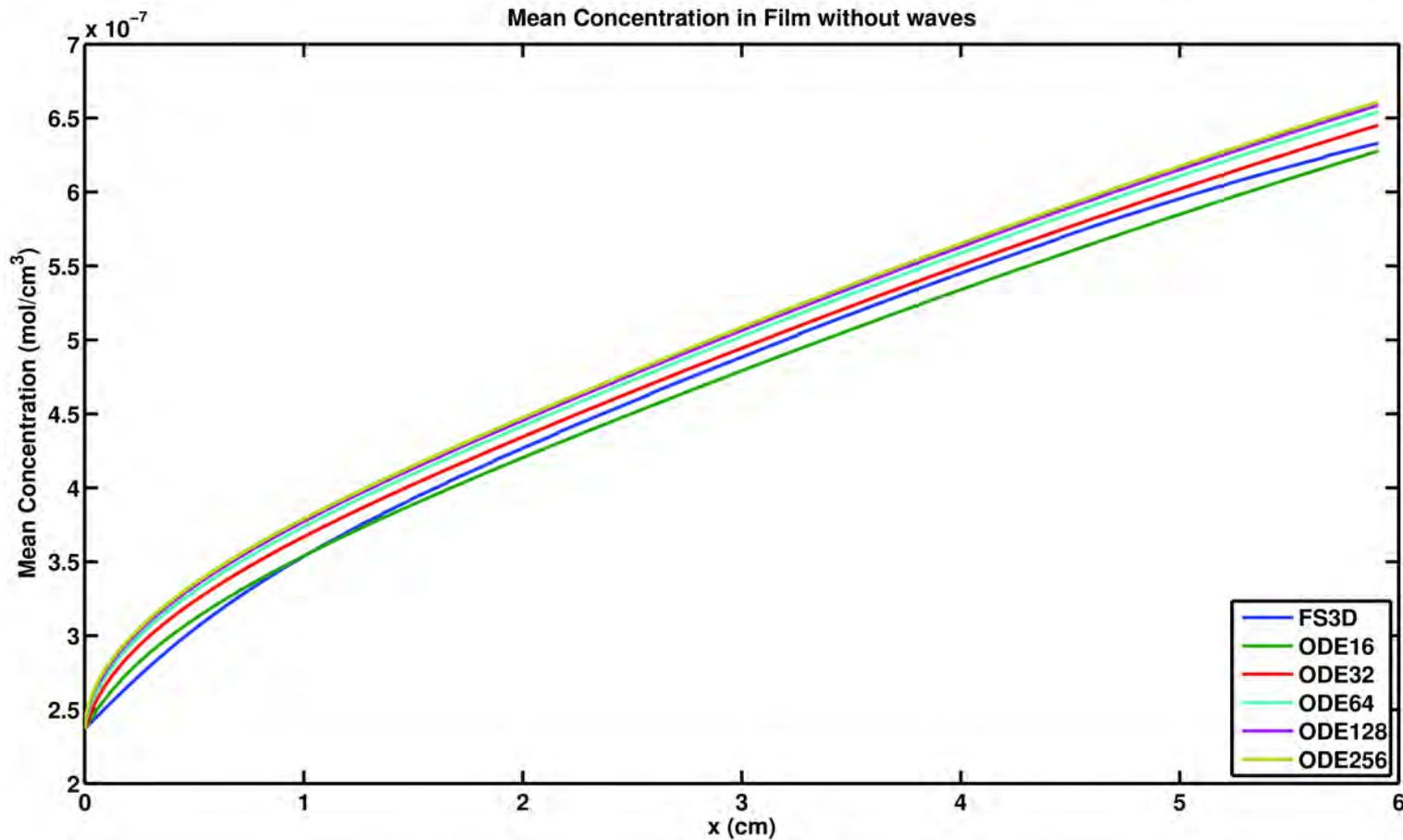
$$c|_{x=0} = c_{L,0}$$

$$\partial_y c|_{y=0} = 0$$

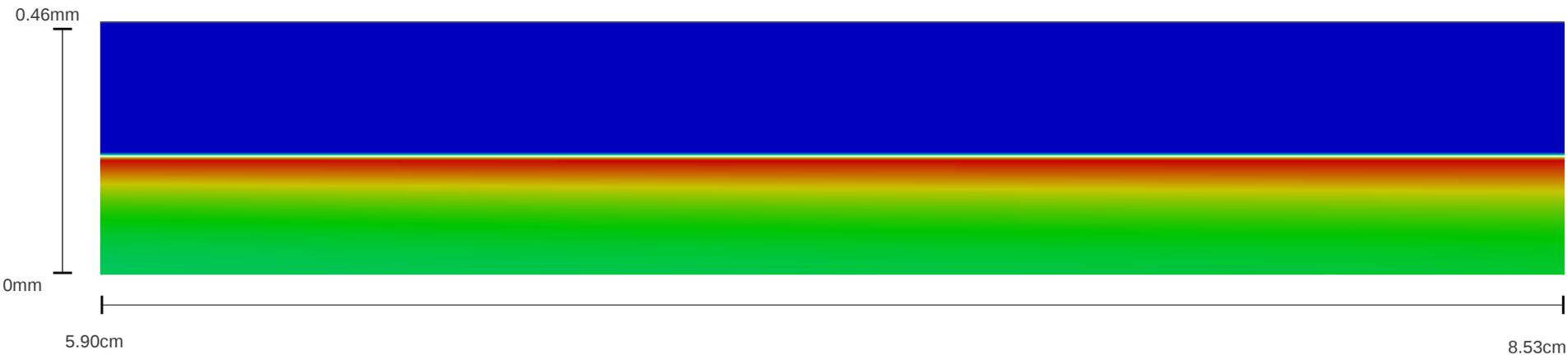
$$\partial_x c|_{x=10\text{cm}} = 0$$

$$\partial_y c|_{y=\delta_0} = k_{H,cc} c_G$$

Validation: Result



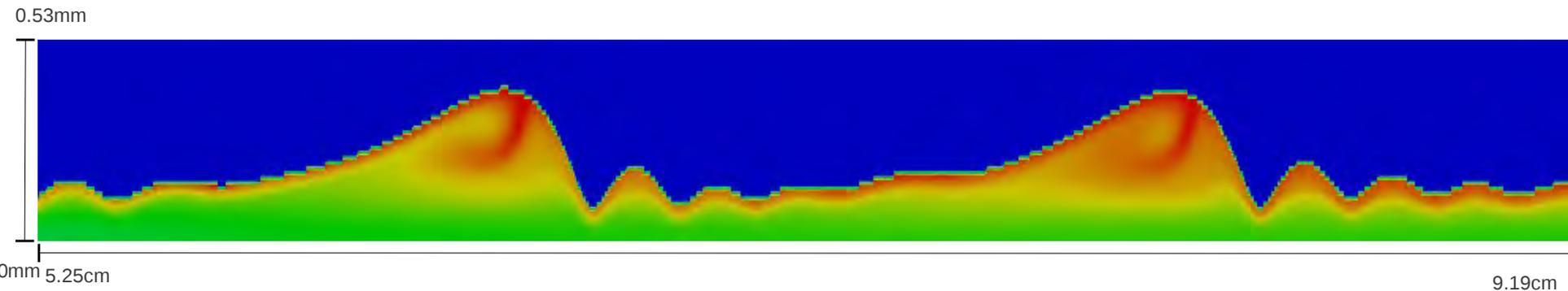
0 Hz



Planar Interface
Pure Diffusion



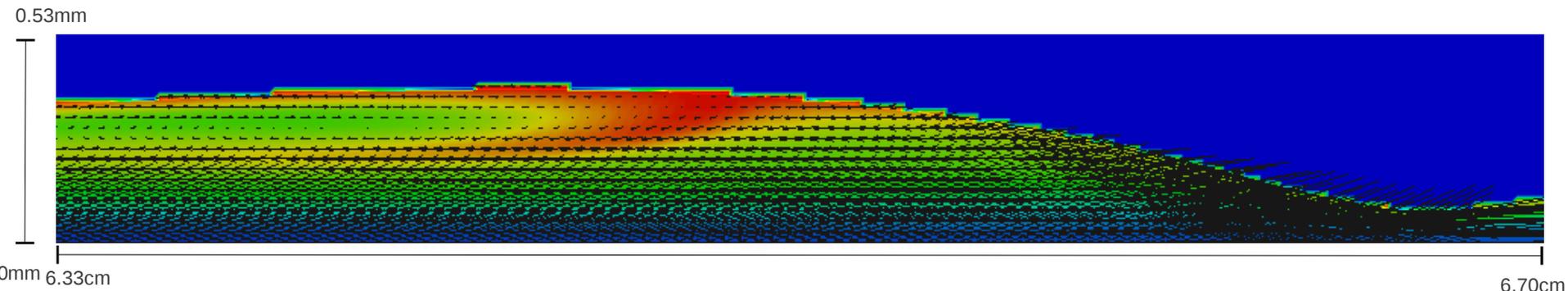
20 Hz



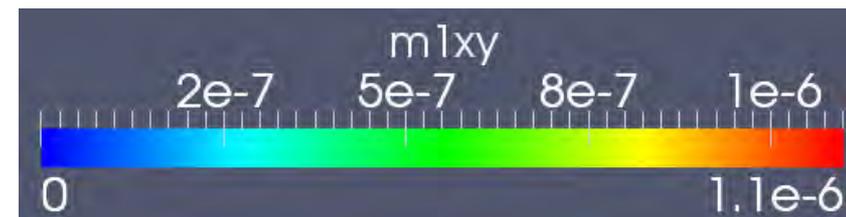
- Time-periodic wave structures appear
- Large Wave humps, preceded by several smaller capillary waves

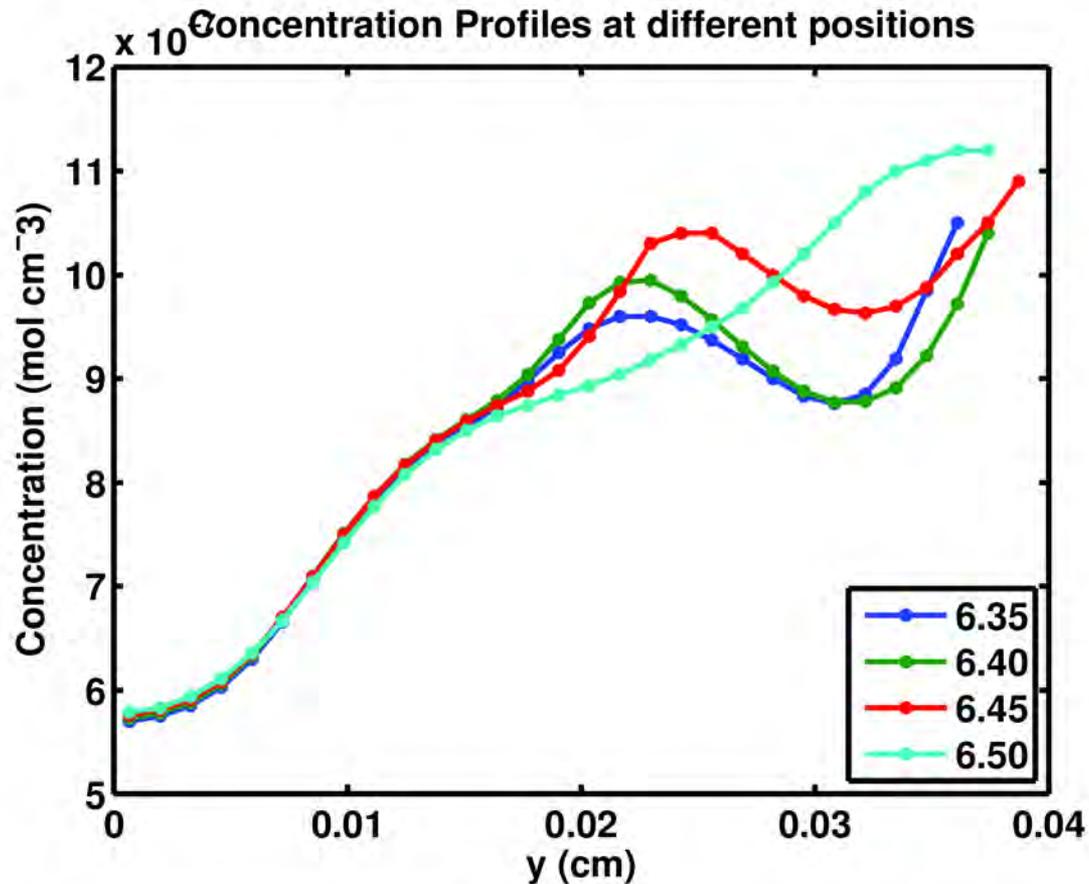


20 Hz



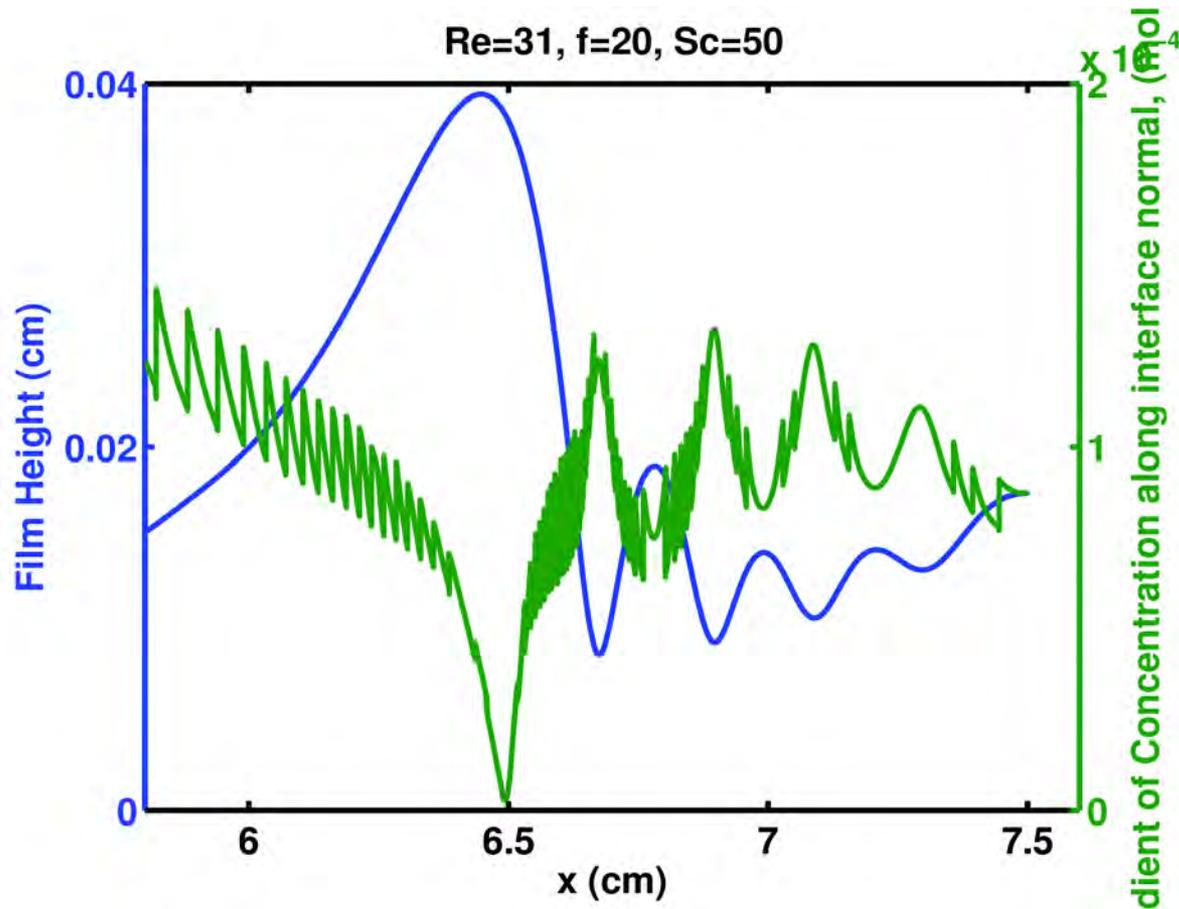
- Filaments of high concentration in the large wave humps
- Develop along the streamlines of the large vortex
- Touch the interface at a hyperbolic point





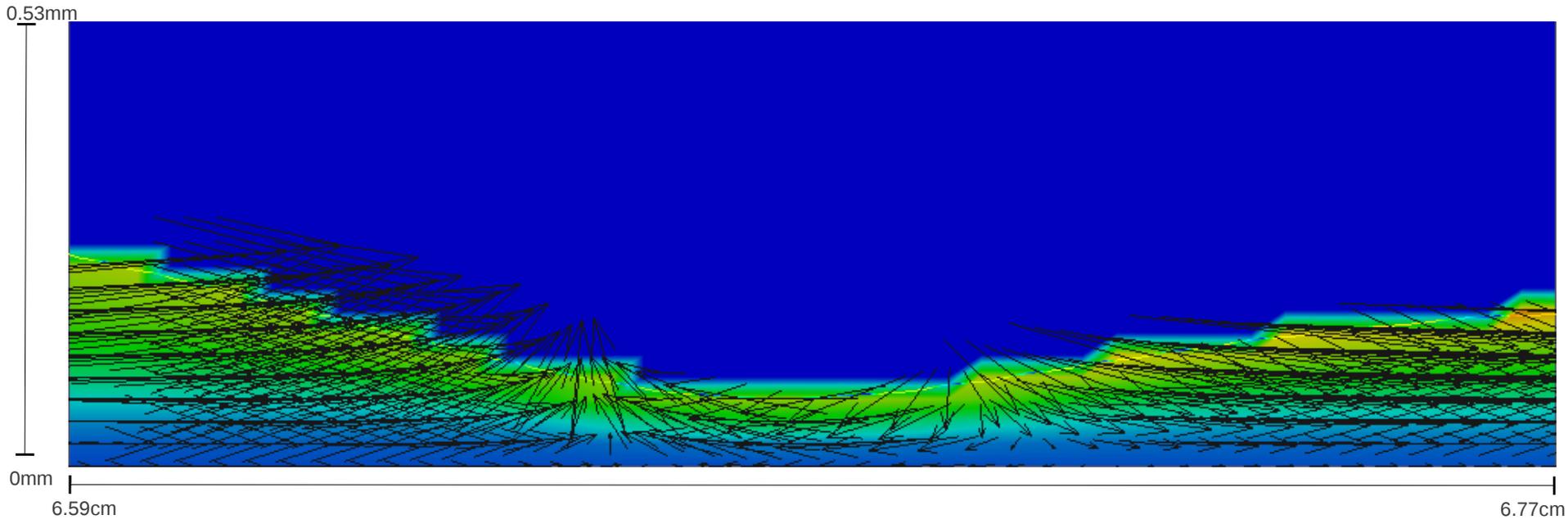
- Highly non-monotonous concentration profiles

20 Hz



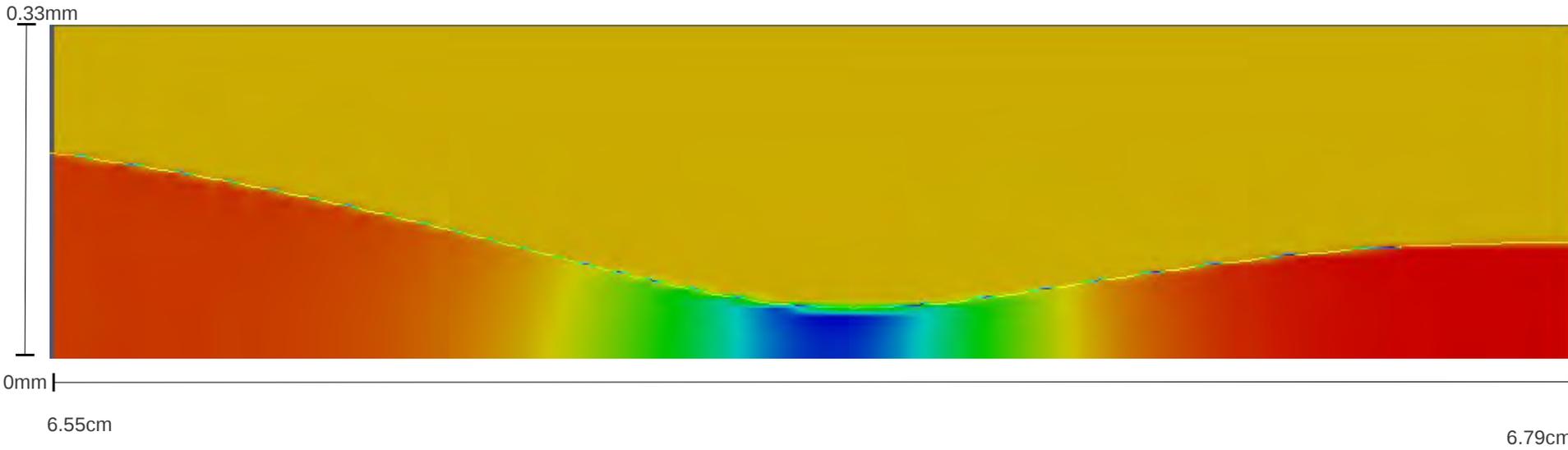
- Strong contribution from the capillary wave region

20 Hz



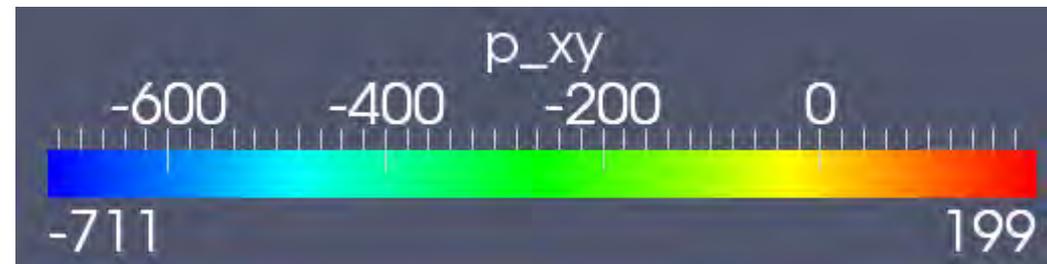
- Flow up the wall in the reference frame of the wall

20 Hz



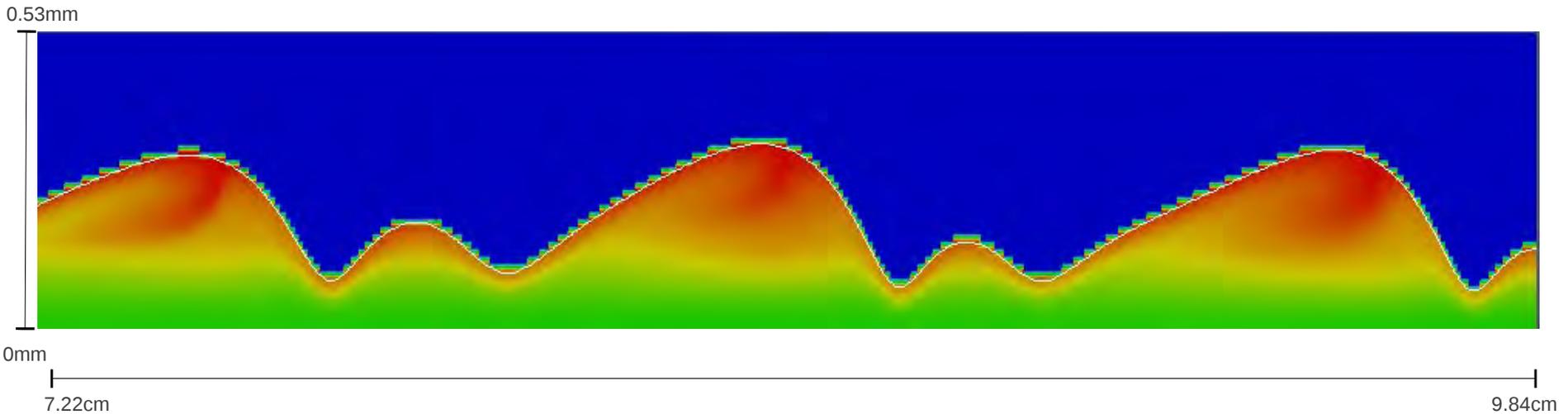
Pressure in film according to Young-Laplace: $\Delta p \sim \sigma \kappa$

Increase in pressure large enough to drive water up the wall



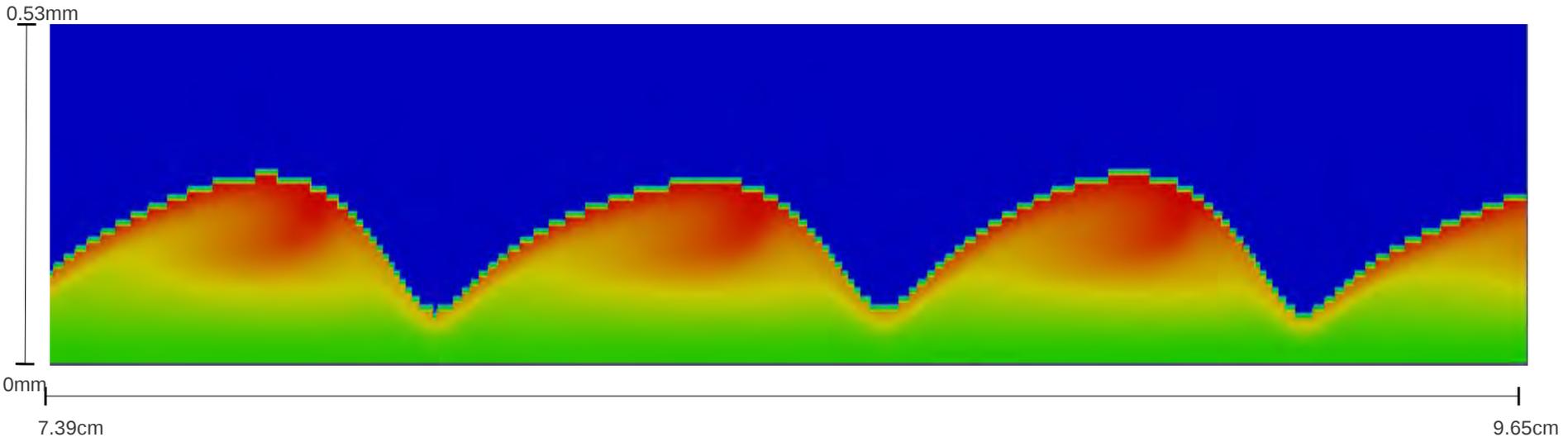
Compare Dietze et al., J. Fluid Mech., 637, 2009

30 Hz



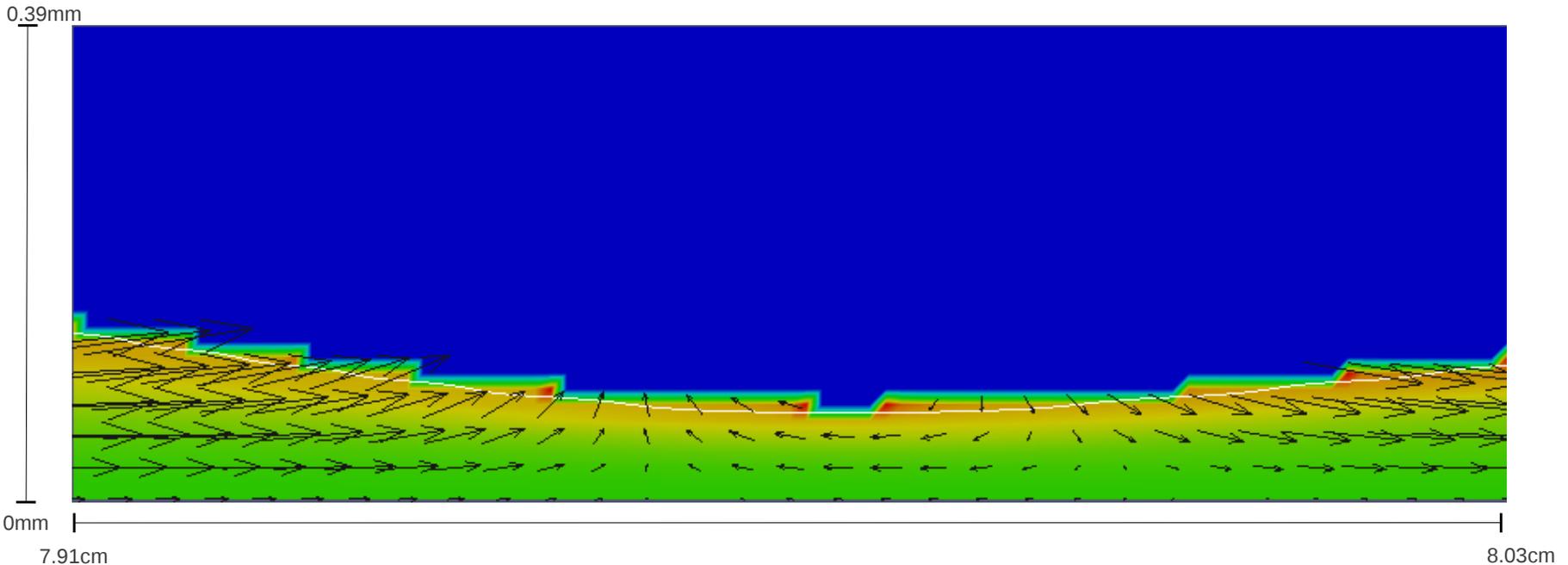
- Less capillary waves
- Wave length, peak height, and wave velocity decrease

40 Hz



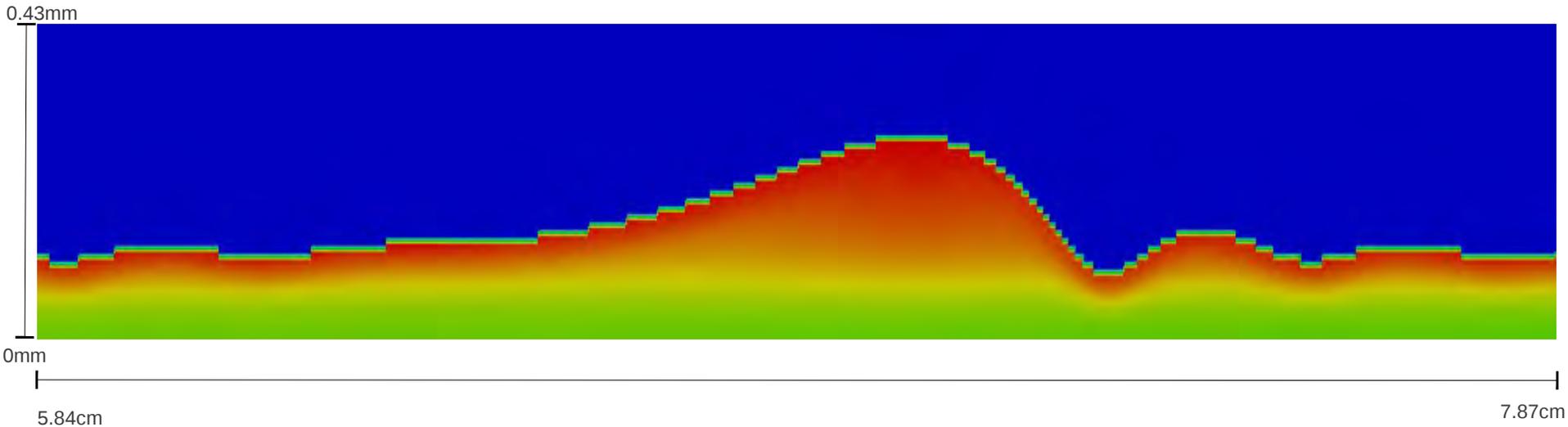
- No capillary waves; waves become sinusoidal
- Wave length, peak height, and wave velocity decrease further

40 Hz

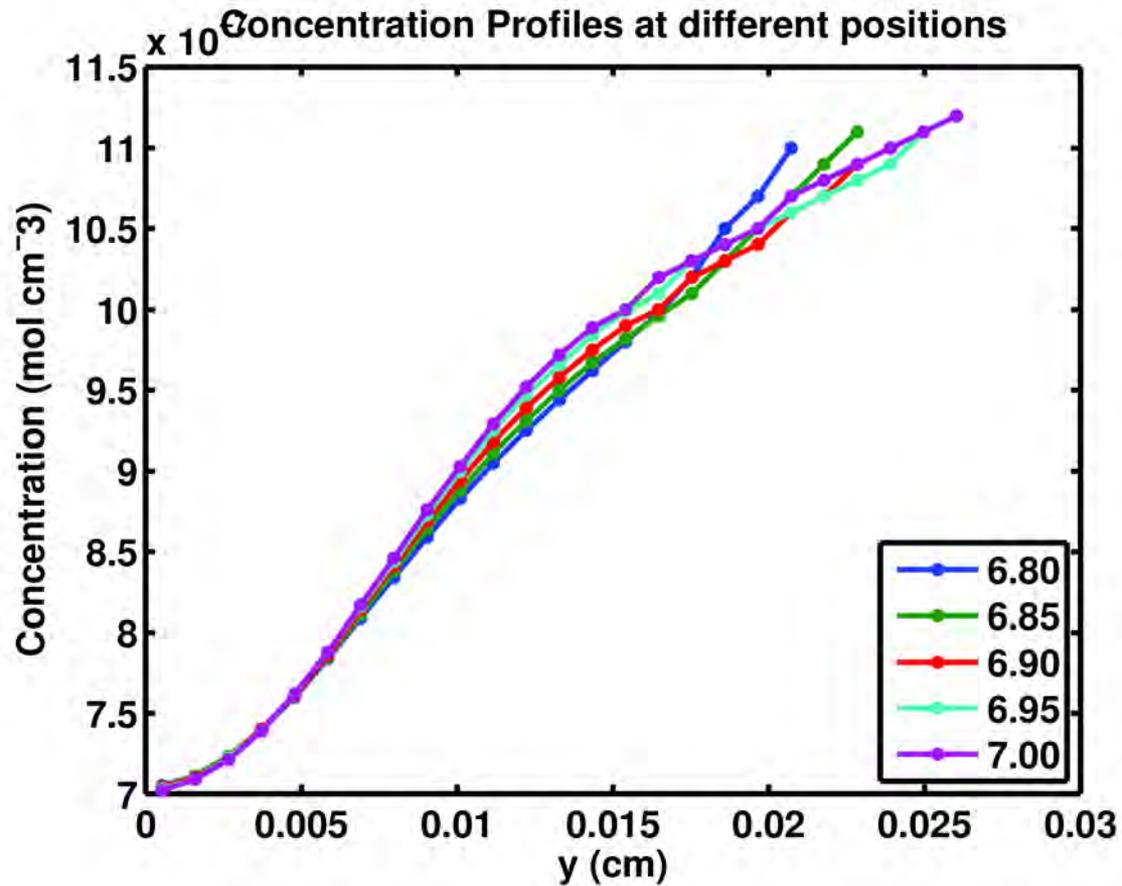


- At this Reynolds Number, there exists backflow even when Capillary Waves are absent

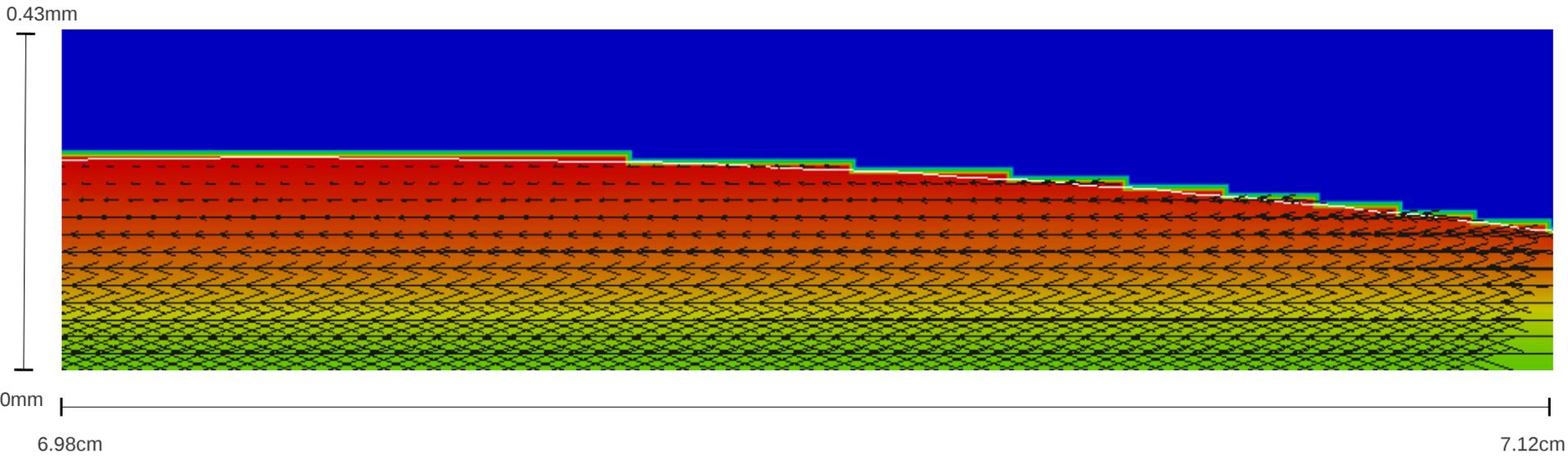
Re 15 / 15Hz



- At this Reynolds Number, concentration profiles are monotonous



Re 15 / 15Hz



- No Vortex relative to wave velocity

Thank you for your attention!