



JOHANNES GUTENBERG
UNIVERSITÄT MAINZ

FSI with Application in Hemodynamics Analysis and Simulation

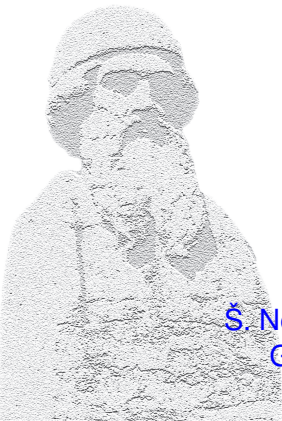
Mária Lukáčová

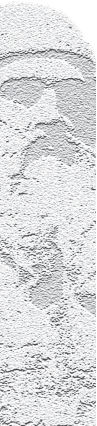
Institute of Mathematics, University of Mainz

A. Hundertmark (Uni-Mainz)

Š. Nečasová (Academy of Sciences, Prague)

G. Rusnáková (Uni-Košice/Uni-Mainz)

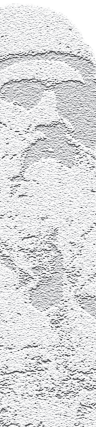




II. Numerical Modelling

Numerical schemes for the FSI problems

- **strong coupled schemes** (inner subiterations or fully composite schemes)
- **weakly coupled schemes** (no subiterations needed)

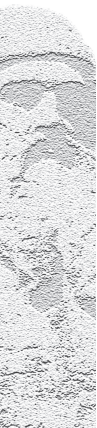


Numerical schemes for the FSI problems

- **strong coupled schemes** (inner subiterations or fully composite schemes)
- **weakly coupled schemes** (no subiterations needed)

- for aerodynamical problems: weakly coupled schemes:
OK

- for biomechanical problems: kind of stronger coupling,
subiterations are typically needed



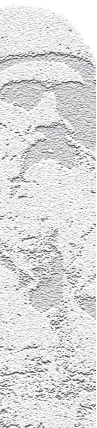
Numerical schemes for the FSI problems

- **strong coupled schemes** (inner subiterations or fully composite schemes)
- **weakly coupled schemes** (no subiterations needed)

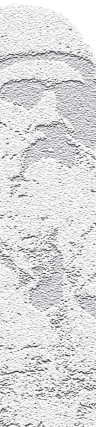
- for aerodynamical problems: weakly coupled schemes: OK

- for biomechanical problems: kind of stronger coupling, subiterations are typically needed

- many numerical approaches for the FSI: immersed boundary, Lagrangian, **Arbitrary Eulerian-Lagrangian (ALE)**



- 1 Quarteroni, Formaggia, Veneziani, Nobile et al. ('01-'07) ... inner subiterations



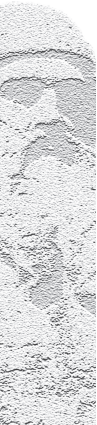
FSI for hemodynamical applications

- 1 Quarteroni, Formaggia, Veneziani, Nobile et al. ('01-'07) ... inner subiterations
- 2 Hron, Turek et al. ('09) monolithic scheme (strong coupling)

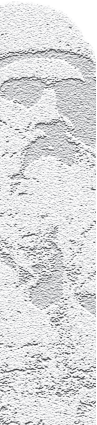


FSI for hemodynamical applications

- 1 Quarteroni, Formaggia, Veneziani, Nobile et al. ('01-'07) ... inner subiterations
- 2 Hron, Turek et al. ('09) monolithic scheme (strong coupling)
- 3 Guidoboni, Glowinski, Cavallini, Čanič ('09): weak coupling: **kinematical coupling**

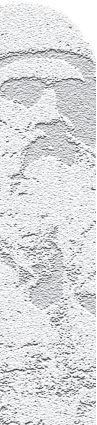


- 1 Quarteroni, Formaggia, Veneziani, Nobile et al. ('01-'07) ... inner subiterations
- 2 Hron, Turek et al. ('09) monolithic scheme (strong coupling)
- 3 Guidoboni, Glowinski, Cavallini, Čanič ('09): weak coupling: **kinematical coupling**
- 4 Janela, Moura, Sequeira ('10): simulations for non-Newtonian FSI



FSI for hemodynamical applications

- 1 Quarteroni, Formaggia, Veneziani, Nobile et al. ('01-'07) ... inner subiterations
- 2 Hron, Turek et al. ('09) monolithic scheme (strong coupling)
- 3 Guidoboni, Glowinski, Cavallini, Čanič ('09): weak coupling: **kinematical coupling**
- 4 Janela, Moura, Sequeira ('10): simulations for non-Newtonian FSI
- 5 Hundertmark, Lukáčová, Rusnáková ('08,'10, '11): analysis and simulations for non-Newtonian FSI schemes (**global and kinematical coupling**)



Numerical methods

- Discretization

- FSI

Stability

- Energy estimates

- Energy estimate for the A operator

- Energy estimates for B operator

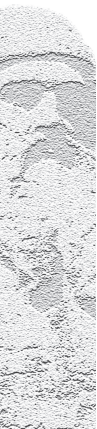
Numerical experiments

- Inflow data and parameters

- Experiment I: stenotic vessel

- Experiment II: bifurcation vessel

Convergence study



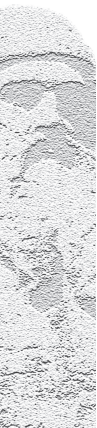
- Fluid equations
 - UG software toolbox



- **Fluid equations**
 - UG software toolbox
 - FV-type schemes



- Fluid equations
 - UG software toolbox
 - FV-type schemes
 - pseudo compressibility stabilization

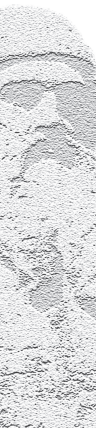


- Fluid equations
 - UG software toolbox
 - FV-type schemes
 - pseudo compressibility stabilization
 - Newton/fixed point linearization of convective term



- Fluid equations
 - UG software toolbox
 - FV-type schemes
 - pseudo compressibility stabilization
 - Newton/fixed point linearization of convective term
- fixed point iterations of non-linear viscosity

$$\mu(|D(\nabla \mathbf{u})|)D(\nabla \mathbf{u}) \approx \mu(|D(\nabla \mathbf{u}^{old})|)D(\nabla \mathbf{u})$$



- **Fluid equations**
 - UG software toolbox
 - FV-type schemes
 - pseudo compressibility stabilization
 - Newton/fixed point linearization of convective term
- fixed point iterations of non-linear viscosity

$$\mu(|D(\nabla \mathbf{u})|)D(\nabla \mathbf{u}) \approx \mu(|D(\nabla \mathbf{u}^{old})|)D(\nabla \mathbf{u})$$

- **Structure equation**

$$\frac{\partial^2 \eta}{\partial t^2} - a \frac{\partial^2 \eta}{\partial x_1^2} + b(1/\eta)\eta - c \frac{\partial^3 \eta}{\partial x_1^2 \partial t} = RHS(u, p, R_0)$$

- finite difference method in time (Newmark scheme)
- finite difference method in space (central approximations)
- ... **second order**

Numerical methods

Discretization

FSI

Stability

Energy estimates

Energy estimate for the A operator

Energy estimates for B operator

Numerical experiments

Inflow data and parameters

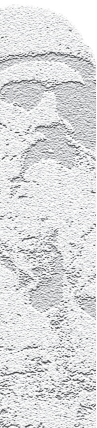
Experiment I: stenotic vessel

Experiment II: bifurcation vessel

Convergence study



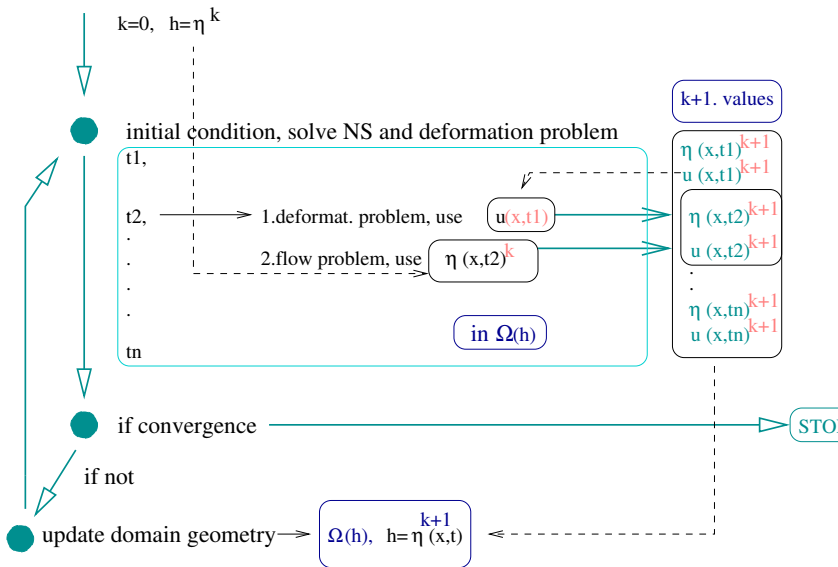
- I. Strong coupling - global iteration method $k=1,2, \dots$
 - solve fluid eq. & structure eq. on the domain $\Omega(\eta^k)$ for $t^n, n = 1, 2, 3 \dots$
 - homogeneous Dirichlet or Neumann boundary conditions



- I. Strong coupling - global iteration method $k=1,2, \dots$
 - solve fluid eq. & structure eq. on the domain $\Omega(\eta^k)$ for $t^n, n = 1, 2, 3 \dots$
 - homogeneous Dirichlet or Neumann boundary conditions
- $(\xi = \partial_t \eta)$

$$\begin{aligned} & \frac{\xi^{n+1} - \xi^n}{\Delta t} - a\alpha \frac{\partial^2 \eta^{n+1}}{\partial x_1^2} + b\alpha \eta^{n+1} - c\alpha \frac{\partial^2 \xi^{n+1}}{\partial x_1^2} \\ &= RHS(p^n, u^n, R_0) + (1 - \alpha) \left(a \frac{\partial^2 \eta^n}{\partial x_1^2} - b\eta^n + c \frac{\partial^2 \xi^n}{\partial x_1^2} \right) \\ & \frac{\eta^{n+1} - \eta^n}{\Delta t} = \alpha \xi^{n+1} + (1 - \alpha) \xi^n, \quad \alpha = 0.5 \end{aligned}$$

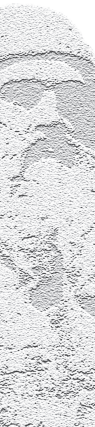
Global iteration with respect to the domain



II. Kinematical coupling [Guidoboni et al. ('09)]

- solve Fluid eq. + Structure eq. on $\Omega(\eta^n)$ for $t \in [t^n, t^{n+1}]$
- **split structure eq.** into 2 parts
- kinematical lateral B.C.

$$u_2|_{y=H} = \frac{\partial \eta}{\partial t} = \xi$$



II. Kinematical coupling [Guidoboni et al. ('09)]

- solve Fluid eq. + Structure eq. on $\Omega(\eta^n)$ for $t \in [t^n, t^{n+1}]$
- **split structure eq.** into 2 parts
- kinematical lateral B.C.

$$u_2|_{y=H} = \frac{\partial \eta}{\partial t} = \xi$$

• 1. hydrodynamic part

fluid eq. + $\xi = u_2|_{y=H}$

$$\frac{\partial \xi}{\partial t} = c \frac{\partial^2 \xi}{\partial x_1^2} + RHS(u, p)$$

• 2. elastic part

$$\frac{\partial \eta}{\partial t} = \xi$$

$$\frac{\partial \xi}{\partial t} = a \frac{\partial^2 \eta}{\partial x_1^2} - b(1/\eta)\eta + RHS(R_0)$$



- Kinematical coupling / Discretization

A operator: hydrodynamic part

Fluid solver +

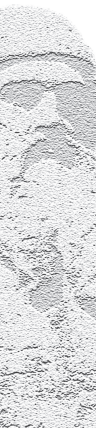
$$\frac{\xi^{n+1/2} - \xi^n}{\Delta t} - c\alpha \frac{\partial^2 \xi^{n+1/2}}{\partial x_1^2} = RHS(p^n, u^n) + c(1 - \alpha) \frac{\partial^2 \xi^n}{\partial x_1^2},$$

B operator: elastic part

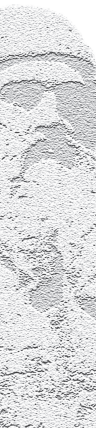
$$\frac{\eta^{n+1} - \eta^n}{\Delta t} = \beta \xi^{n+1} + (1 - \beta) \xi^{n+1/2}, \quad \beta = 0.5$$

$$\begin{aligned} \frac{\xi^{n+1} - \xi^{n+1/2}}{\Delta t} - a\alpha \frac{\partial^2 \eta^{n+1}}{\partial x_1^2} + b(1/\eta^n) \alpha \eta^{n+1} \\ = RHS(R_0) + a(1 - \alpha) \frac{\partial^2 \eta^n}{\partial x_1^2} - b(1/\eta^n)(1 - \alpha) \eta^n \quad \alpha = 1, 0.5 \end{aligned}$$

- kinematical splitting scheme of the **Marchuk-Yanenko type**
 - 1st order accurate
 - $A_{\Delta t} \curvearrowright B_{\Delta t}$
in the $(n + 1)$ – th time-step on $\Omega(t^n)$



- kinematical splitting scheme of the **Marchuk-Yanenko type**
 - 1st order accurate
 - $A_{\Delta t} \curvearrowright B_{\Delta t}$
in the $(n + 1)$ – th time-step on $\Omega(t^n)$
- kinematical splitting scheme of the **Strang-type kinematical splitting**
 - 2nd order accurate
 - $B_{\Delta t/2} \curvearrowright A_{\Delta t} \curvearrowright B_{\Delta t/2}$
in the $(n + 1)$ – th time-step on $\Omega(t^n)$



Numerical methods

Discretization

FSI

Stability

Energy estimates

Energy estimate for the A operator

Energy estimates for B operator

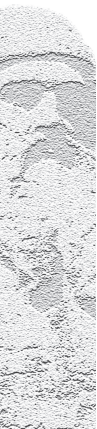
Numerical experiments

Inflow data and parameters

Experiment I: stenotic vessel

Experiment II: bifurcation vessel

Convergence study



Arbitrary Lagrangian-Eulerian Mapping

$$\mathcal{A}_t : \Omega_0 \rightarrow \Omega_t$$

$$\mathcal{A}_t(\mathbf{X}) = \mathbf{x} \in \Omega_t$$

$$f(t, \mathbf{x}) \equiv \tilde{f}(t, \mathcal{A}_t^{-1} \mathbf{x}) \equiv \tilde{f}(t, \mathbf{X})$$

$\frac{\mathcal{D}^A \mathbf{u}}{\mathcal{D}t}$ ALE derivative

$\mathbf{w} := \frac{\partial \mathbf{x}}{\partial t}$ "grid velocity"

$$\begin{aligned} \frac{\mathcal{D}^A \mathbf{u}(t, \mathbf{x})}{\mathcal{D}t} &:= \frac{\partial \tilde{\mathbf{u}}(t, \mathbf{X})}{\partial t} \\ &= \frac{\partial \mathbf{u}(t, \mathbf{x})}{\partial t} + \mathbf{w} \cdot \nabla \mathbf{u}(t, \mathbf{x}) \end{aligned}$$

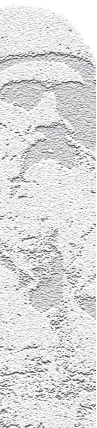
Weak formulation of coupled problem

- test functions: $\mathbf{v} \in V$, where

$$V \equiv \left\{ \mathbf{v} \in W^{1,p}(\Omega(t))^2 : v_1|_{\Gamma_{wall}} = 0, v_2|_{x_2=0} = 0 \right\}$$

$\frac{\mathcal{D}^A \mathbf{u}}{\mathcal{D}t}$ ALE derivative $\mathbf{w} := \frac{\partial \mathbf{X}}{\partial t}$ grid velocity

$$\frac{\mathcal{D}^A \mathbf{u}}{\mathcal{D}t} := \frac{\partial \mathbf{u}}{\partial t} + \mathbf{w} \cdot \nabla \mathbf{u}(\mathbf{x}, t)$$




Weak formulation of coupled problem

- test functions: $\mathbf{v} \in \mathbf{V}$, where

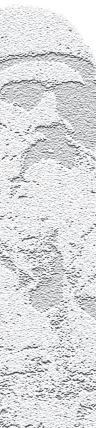
$$\mathbf{V} \equiv \left\{ \mathbf{v} \in W^{1,p}(\Omega(t))^2 : v_1|_{\Gamma_{wall}} = 0, v_2|_{x_2=0} = 0 \right\}$$

$\frac{\mathcal{D}^A \mathbf{u}}{\mathcal{D}t}$ ALE derivative $\mathbf{w} := \frac{\partial \mathbf{x}}{\partial t}$ grid velocity

$$\frac{\mathcal{D}^A \mathbf{u}}{\mathcal{D}t} := \frac{\partial \mathbf{u}}{\partial t} + \mathbf{w} \cdot \nabla \mathbf{u}(\mathbf{x}, t)$$


$$\begin{aligned} & \int_{\Omega(t)} \frac{\mathcal{D}^A \mathbf{u}}{\mathcal{D}t} \mathbf{v} \, d\mathbf{x} + \int_{\Omega(t)} ((\mathbf{u} - \mathbf{w}) \cdot \nabla \mathbf{u}) \mathbf{v} \, d\mathbf{x} - \\ & \int_{\Omega(t)} \rho \operatorname{div} \mathbf{v} \, d\mathbf{x} + \frac{1}{\rho} \int_{\Omega(t)} 2\mu(|\mathbf{D}(\mathbf{u})|) \mathbf{D}(\mathbf{u}) : \mathbf{D}(\mathbf{v}) \, d\mathbf{x} + \\ & \int_0^L \left(\frac{\partial^2 \eta}{\partial t^2} + b\eta \right) v_2|_{\Gamma_{wall}} \, dx_1 + \int_0^L \left(a \frac{\partial \eta}{\partial x_1} + c \frac{\partial^2 \eta}{\partial t \partial x_1} \right) \frac{\partial (v_2|_{\Gamma_{wall}})}{\partial x_1} \\ & = \int_0^{R_0} P_{in} v_1|_{x_1=0} \, dx_2, \quad \forall \mathbf{v} \in \mathbf{V}, \text{ a.e. } t \in I. \end{aligned}$$

- with G. Rusnáková
 - weak formulation of the semi-discrete coupled problem
 - $p \geq 2$
 - test with \mathbf{u}^{n+1}
 - kinematic pressure boundary conditions on infow / outflow
 - symmetry boundary conditions $x_2 = 0$



Numerical methods

Discretization

FSI

Stability

Energy estimates

Energy estimate for the A operator

Energy estimates for B operator

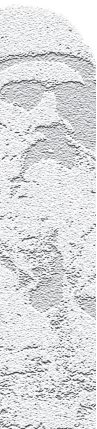
Numerical experiments

Inflow data and parameters

Experiment I: stenotic vessel

Experiment II: bifurcation vessel

Convergence study



$$\begin{aligned} & \frac{1}{2} \|\mathbf{u}^{n+1}\|_{L^2(\Omega(t_{n+1}))}^2 + \frac{c^*}{2\rho} \Delta t \|\mathbf{u}^{n+1}\|_{W^{1,2}(\Omega(t_{n+1/2}))}^2 \\ & + \frac{1}{2} \|\xi^{n+1/2}\|_{L^2(0,L)}^2 + c\Delta t \|\xi_x^{n+1/2}\|_{L^2(0,L)}^2 \leq \\ & \leq \frac{1}{2} \|\mathbf{u}^n\|_{L^2(\Omega(t_n))}^2 + \frac{1}{2} \|\xi^n\|_{L^2(0,L)}^2 + c\Delta t |P_{in}^{n+1}|^2 \end{aligned}$$

- we obtain the following estimate for the A-operator

$$\begin{aligned} & \|\xi^{n+1/2}\|_{L^2(0,L)}^2 + \|\mathbf{u}^{n+1}\|_{L^2(\Omega(t_{n+1}))}^2 \\ & \leq \|\xi^n\|_{L^2(0,L)}^2 + \|\mathbf{u}^n\|_{L^2(\Omega(t_n))}^2 + 2c\Delta t |P_{in}^{n+1}|^2 \end{aligned}$$

Numerical methods

Discretization

FSI

Stability

Energy estimates

Energy estimate for the A operator

Energy estimates for B operator

Numerical experiments

Inflow data and parameters

Experiment I: stenotic vessel

Experiment II: bifurcation vessel

Convergence study

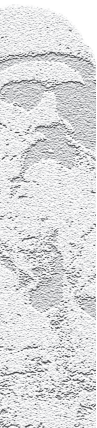


Energy of A-operator:

$$\begin{aligned} & \|\xi^{n+\frac{1}{2}}\|_{L^2(0,L)}^2 \leq \|\xi^n\|_{L^2(0,L)}^2 + \|\mathbf{u}^n\|_{L^2(\Omega(t_n))}^2 - \|\mathbf{u}^{n+1}\|_{L^2(\Omega(t_{n+1}))}^2 \\ & + 2c\Delta t |P_{in}^{n+1}|^2 \end{aligned}$$

Energy of B-operator:

$$\begin{aligned} & a \|\eta_{x_1}^{N+1}\|_{L^2(0,L)}^2 + b \|\eta^{N+1}\|_{L^2(0,L)}^2 + \|\xi^{N+1}\|_{L^2(0,L)}^2 \\ & = a \|\eta_{x_1}^0\|_{L^2(0,L)}^2 + b \|\eta^0\|_{L^2(0,L)}^2 + \|\xi^0\|_{L^2(0,L)}^2 \\ & + \sum_{n=0}^N \left(\|\xi^{n+\frac{1}{2}}\|_{L^2(0,L)}^2 - \|\xi^n\|_{L^2(0,L)}^2 \right) \end{aligned}$$



Energy of the solution

Energy of A-operator:

$$\begin{aligned} \|\xi^{n+\frac{1}{2}}\|_{L^2(0,L)}^2 &\leq \|\xi^n\|_{L^2(0,L)}^2 + \|\mathbf{u}^n\|_{L^2(\Omega(t_n))}^2 - \|\mathbf{u}^{n+1}\|_{L^2(\Omega(t_{n+1}))}^2 \\ &+ 2c\Delta t |P_{in}^{n+1}|^2 \end{aligned}$$

Energy of B-operator:

$$\begin{aligned} &a \|\eta_{x_1}^{N+1}\|_{L^2(0,L)}^2 + b \|\eta^{N+1}\|_{L^2(0,L)}^2 + \|\xi^{N+1}\|_{L^2(0,L)}^2 \\ &= a \|\eta_{x_1}^0\|_{L^2(0,L)}^2 + b \|\eta^0\|_{L^2(0,L)}^2 + \|\xi^0\|_{L^2(0,L)}^2 \\ &\quad + \sum_{n=0}^N \left(\|\xi^{n+\frac{1}{2}}\|_{L^2(0,L)}^2 - \|\xi^n\|_{L^2(0,L)}^2 \right) \end{aligned}$$

Energy estimate of the solution:

$$E^{N+1} \leq E^0 + \sum_{n=0}^N 2c\Delta t |P_{in}^{n+1}|^2$$

$$E^k = \|\mathbf{u}^k\|_{L^2(\Omega(t_k))}^2 + a \|\eta_{x_1}^k\|_{L^2(0,L)}^2 + b \|\eta^k\|_{L^2(0,L)}^2 + \|\xi^k\|_{L^2(0,L)}^2$$

Numerical methods

Discretization

FSI

Stability

Energy estimates

Energy estimate for the A operator

Energy estimates for B operator

Numerical experiments

Inflow data and parameters

Experiment I: stenotic vessel

Experiment II: bifurcation vessel

Convergence study



✓ *Wall Shear Stress*

$$WSS := \tau_w = -\mathbf{T}_f \mathbf{n} \cdot \boldsymbol{\tau}, \quad (1)$$

negative values of the WSS - indicate existence of large recirculation zones

● *Oscillatory Shear Index*

$$OSI := \frac{1}{2} \left(1 - \frac{\int_0^T \tau_w dt}{\int_0^T |\tau_w| dt} \right), \quad (2)$$

measures temporal oscillations of the shear stress pointwisely - indicates areas with large stenotic plug danger

● Reynolds number

$$RE_0 = \frac{\rho V l}{\mu_0} \quad \text{or} \quad RE_\infty = \frac{\rho V l}{\mu_\infty} \quad \text{or} \quad RE = \frac{\rho V l}{\frac{1}{2}(\mu_0 + \mu_\infty)}$$

✓ *Wall Shear Stress*

$$WSS := \tau_w = -\mathbf{T}_f \mathbf{n} \cdot \boldsymbol{\tau}, \quad (1)$$

negative values of the WSS - indicate existence of large recirculation zones

✓ *Oscillatory Shear Index*

$$OSI := \frac{1}{2} \left(1 - \frac{\int_0^T \tau_w dt}{\int_0^T |\tau_w| dt} \right), \quad (2)$$

measures temporal oscillations of the shear stress pointwisely - indicates areas with large stenotic plug danger

● Reynolds number

$$RE_0 = \frac{\rho V l}{\mu_0} \quad \text{or} \quad RE_\infty = \frac{\rho V l}{\mu_\infty} \quad \text{or} \quad RE = \frac{\rho V l}{\frac{1}{2}(\mu_0 + \mu_\infty)}$$

✓ *Wall Shear Stress*

$$WSS := \tau_w = -\mathbf{T}_f \mathbf{n} \cdot \boldsymbol{\tau}, \quad (1)$$

negative values of the WSS - indicate existence of large recirculation zones

✓ *Oscillatory Shear Index*

$$OSI := \frac{1}{2} \left(1 - \frac{\int_0^T \tau_w dt}{\int_0^T |\tau_w| dt} \right), \quad (2)$$

measures temporal oscillations of the shear stress pointwisely - indicates areas with large stenotic plug danger

✓ **Reynolds number**

$$RE_0 = \frac{\rho V l}{\mu_0} \quad \text{or} \quad RE_\infty = \frac{\rho V l}{\mu_\infty} \quad \text{or} \quad RE = \frac{\rho V l}{\frac{1}{2}(\mu_0 + \mu_\infty)}$$

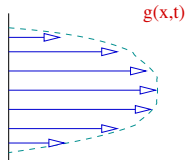


inflow velocity

pulsatile parabolic profile

$$u_{inflow}(-L, x_2) = V(1 - x_2)(1 + x_2) \sin^2(\pi t/\omega) \quad \text{on } \Gamma_{in},$$

or some $f(t)$, e.g., iliac artery measurements



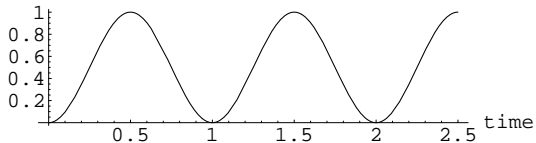
inflow velocity

pulsatile parabolic profile

$$u_{inflow}(-L, x_2) = V(1 - x_2)(1 + x_2) \sin^2(\pi t/\omega) \quad \text{on } \Gamma_{in},$$

or some $f(t)$, e.g., iliac artery measurements

periodic_function



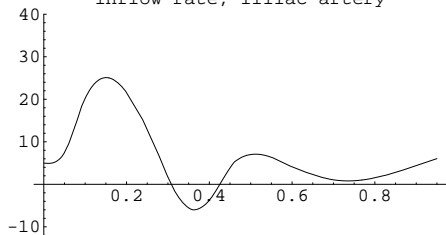
inflow velocity

pulsatile parabolic profile

$$U_{inflow}(-L, x_2) = V(1 - x_2)(1 + x_2) \sin^2(\pi t/\omega) \text{ on } \Gamma_{in},$$

or some $f(t)$, e.g., iliac artery measurements

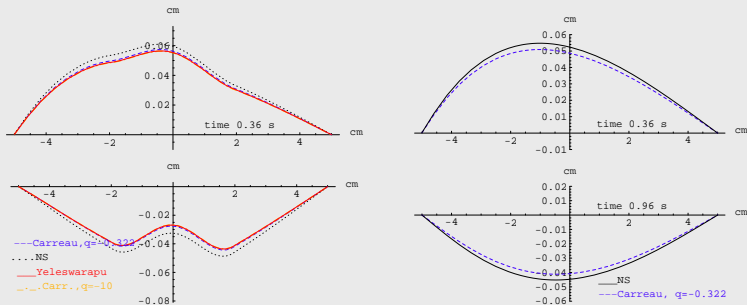
Inflow rate, iliac artery



$$Q(t) = \int_{\Gamma_{in}} \mathbf{u}_{inflow} dx_2 \implies f(t) = Q(t) \frac{3}{4VR(t)}$$

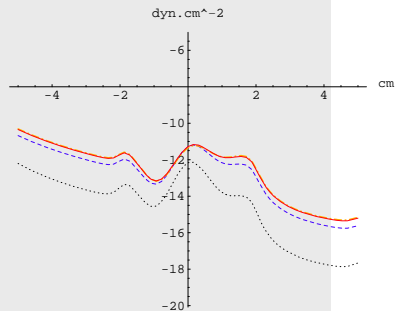
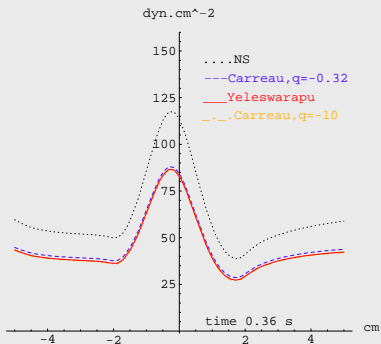
Some hemodynamical quantities

domain deformation: stenosed and straight channel

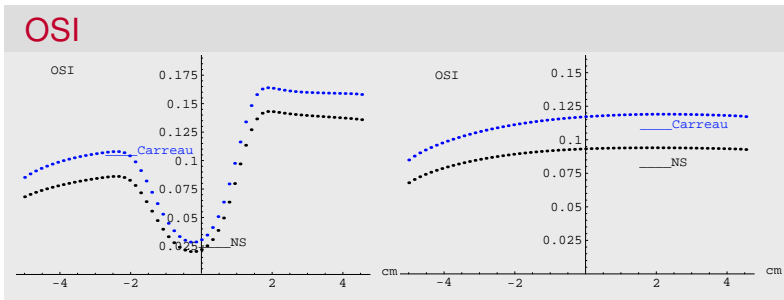
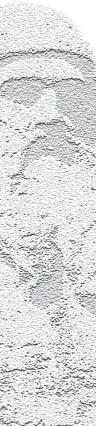


Some hemodynamical quantities

WSS-stenosed channel



Some hemodynamical quantities



M.L. & A. Hundertmark [Comp.& Math.Appl. ('10)]

Numerical methods

Discretization

FSI

Stability

Energy estimates

Energy estimate for the A operator

Energy estimates for B operator

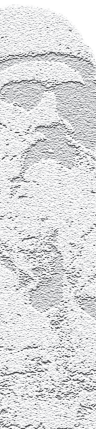
Numerical experiments

Inflow data and parameters

Experiment I: stenotic vessel

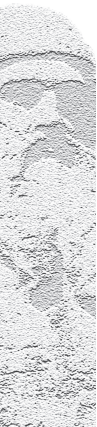
Experiment II: bifurcation vessel

Convergence study



Summary

- 1 **Effects due to complex geometry:**
wall deformation, extrema of WSS, OSI in stenosed / bifurcation regions
- 2 **Effects due to the Non-Newtonian rheology:**
WSS: larger negative absolute value \implies recirculation zones,
OSI: larger extremes \implies more sensible prediction of stenotic plug
- 3 **Difference between Carreau and Yeleswarapu model:**
negligible



- 1 **Effects due to complex geometry:**
wall deformation, extrema of WSS, OSI in stenosed / bifurcation regions
- 2 **Effects due to the Non-Newtonian rheology:**
WSS: larger negative absolute value \implies recirculation zones,
OSI: larger extremes \implies more sensible prediction of stenotic plug
- 3 **Difference between Carreau and Yeleswarapu model:**
negligible
- 4 **FSI & kinematical coupling:** **efficient, stable FSI algorithm**

