

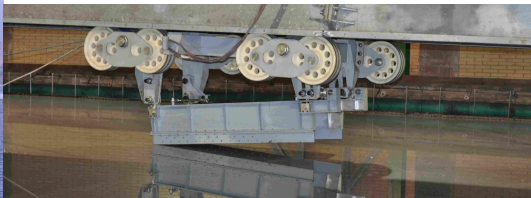
# Water entry at high horizontal speed

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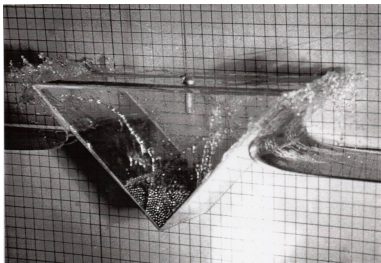
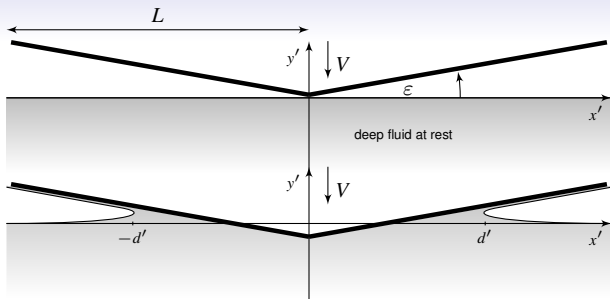
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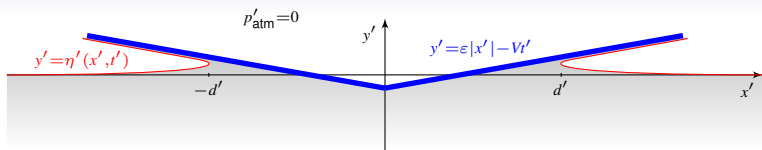
Waseda University



## Wagner model for vertical impact



viscosity,  
surface tension,  
compressibility  
are neglected



Nondimensional variables:

$$x' = Lx, \quad y' = Ly, \quad t' = \frac{\varepsilon L}{V}t, \quad \varphi' = LV\varphi, \quad \eta' = \varepsilon L\eta$$

$$\Delta\varphi(x, y, t) = 0 \quad ((x, y) \in \Omega(t))$$

$$\varphi_y = -1 + \varepsilon\varphi_x \operatorname{sgn}(x) \quad (y = \varepsilon(|x| - t))$$

$$\varphi_y = \eta_t + \varepsilon\eta_x\varphi_x \quad (y = \varepsilon\eta(x, t))$$

$$\varphi_t = -\frac{\varepsilon}{2}|\nabla\varphi|^2 - \frac{\varepsilon gL}{V^2}y \quad (y = \varepsilon\eta(x, t))$$

$$\varphi \rightarrow 0 \quad (x^2 + y^2 \rightarrow \infty)$$

initial conditions:  $\eta(x, 0) = 0, \varphi(x, y, 0) = 0$

Hydrodynamic pressure:  $p = -\varphi_t + \frac{\varepsilon}{2}|\nabla\varphi|^2 - \frac{\varepsilon gL}{V^2}y \quad ((x, y) \in \Omega(t))$

## Leading-order hydrodynamic problem for $\varepsilon \ll 1$

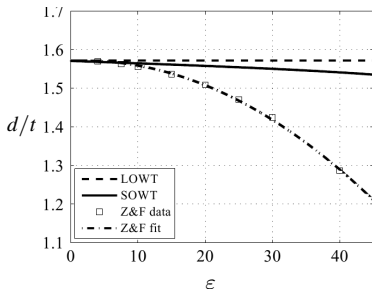
$$\begin{aligned} \Delta\varphi &= 0 & (y < 0) \\ \varphi_y &= -1 & (y = 0, |x| < d) \\ \varphi_y &= \eta_t & (y = 0, |x| > d) \\ \varphi_t &= 0 & (y = 0, |x| > d) \\ \varphi &\rightarrow 0 & (x^2 + y^2 \rightarrow \infty) \\ p &= -\varphi_t & (y = 0, |x| < d) \\ \eta(x, 0) &= 0 & (x \in \mathbb{R}) \end{aligned}$$

Wagner's condition:

$$\eta(d, t) = d - t \quad (d > 0)$$

$$\varphi = O(1) \quad ((x, y) \rightarrow (\pm d, 0))$$

$$\text{Solution: } d(t) = \frac{\pi}{2}t$$

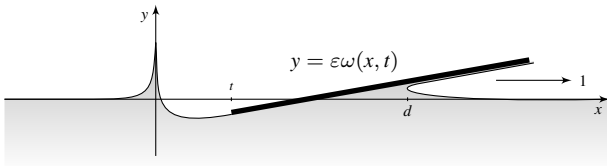
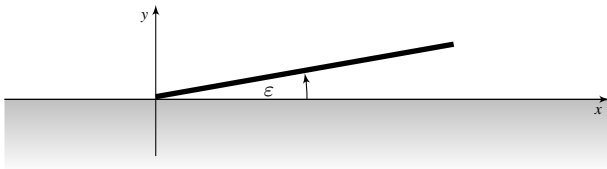


LOWT: Leading order Wagner theory

SOWT: Second order Wagner theory (Oliver, 2007)

Z&F: Numerical solution exploiting self-similarity (Zhao & Faltinsen, 1993)

## Oblique impact of a plate



## Oblique impact of a plate

$$\begin{aligned}\Delta\varphi &= 0 & (y < 0) \\ \varphi_y &= \omega_t(x, t) & (y = 0, t < x < d) \\ \varphi &= 0 & (y = 0, x < 0, x > d) \\ \varphi_x &= A(x) & (y = 0, 0 < x < t) \\ \\ \varphi &\rightarrow 0 & (x^2 + y^2 \rightarrow \infty) \\ \varphi &= O(1) & ((x, y) \rightarrow (d, 0)) \\ |\nabla\varphi| &= O(1) & ((x, y) \rightarrow (t, 0))\end{aligned}$$

where  $d = d(t)$  is given by:

$$\begin{aligned}\omega(d, t) &= \eta(d, t) & (d > t) \\ \varphi_y &= \eta_t & (y = 0, x < t, x > d) \\ \eta(x, 0) &= 0\end{aligned}$$

$$\begin{aligned}\eta(t, t) &= \omega(t, t) \\ p &= -\varphi_t & (y = 0, t < x < d)\end{aligned}$$

$$\text{MBVP} \implies \int_0^t \sqrt{\frac{d-\xi}{t-\xi}} A(\xi) \, d\xi = \int_t^d \sqrt{\frac{d-\xi}{\xi-t}} \omega_t(\xi, t) \, d\xi$$

displacement potential:  $\Phi(x, y, t) = \int_0^\tau \varphi(x, y, \tau) d\tau$

$$\Delta\Phi = 0 \quad (y < 0)$$

$$\Phi_y = \omega(x, t) \quad (y = 0, t < x < d)$$

$$\Phi = 0 \quad (y = 0, x < 0 \text{ and } x > d)$$

$$\Phi_x = tA(x) + B(x) \quad (y = 0, 0 < x < t)$$

$$|\nabla\Phi| = O(1) \quad ((x, y) \rightarrow (t, 0))$$

$$\Phi = O(((x-d)^2 + y^2)^{1/2}) \quad ((x, y) \rightarrow (d, 0))$$

$$\Phi \rightarrow 0 \quad (x^2 + y^2 \rightarrow \infty)$$

$$\int_0^t \sqrt{\frac{t-\xi}{d-\xi}} (tA(\xi) + B(\xi)) d\xi = - \int_t^d \sqrt{\frac{\xi-t}{d-\xi}} \omega(\xi, t) d\xi$$

$$\int_0^t \sqrt{\frac{d-\xi}{t-\xi}} (tA(\xi) + B(\xi)) d\xi = \int_t^d \sqrt{\frac{d-\xi}{\xi-t}} \omega(\xi, t) d\xi$$



$$\int_0^t \sqrt{\frac{d-\xi}{t-\xi}} A(\xi) d\xi = \int_t^d \sqrt{\frac{d-\xi}{\xi-t}} \omega_t(\xi, t) d\xi$$

$$\int_0^t \sqrt{\frac{t-\xi}{d-\xi}} (tA(\xi) + B(\xi)) d\xi = - \int_t^d \sqrt{\frac{\xi-t}{d-\xi}} \omega(\xi, t) d\xi$$

$$\int_0^t \sqrt{\frac{d-\xi}{t-\xi}} (tA(\xi) + B(\xi)) d\xi = \int_t^d \sqrt{\frac{d-\xi}{\xi-t}} \omega(\xi, t) d\xi$$

For rigid-plate impact at constant velocity:

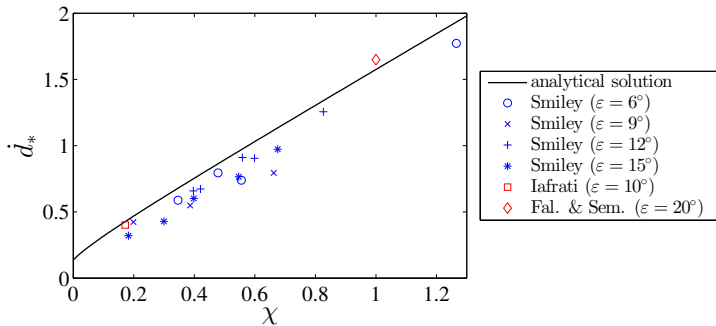
$$\omega(x, t) = x - t(1 + \chi), \quad \chi = \frac{V}{\varepsilon U}$$

⇒ Solution is self-similar solution:  $A(x) = A^*$ ,  $B(x) = B^*x$ ,  $\dot{d}(t) = \dot{d}_*t$

Solution of the problem:

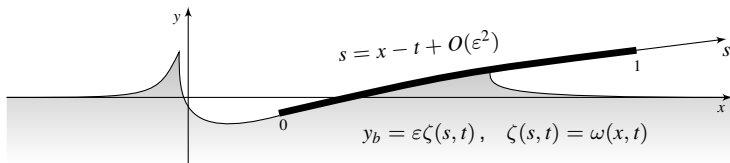
$$\dot{d}_* = q^{-2}, \quad A^* = -\frac{\pi}{4q} \frac{\chi - 1 + 2q^2(1 + 2\chi)}{(q^2 + 1)^{3/2}}, \quad B^* = -A^* \frac{4q^2 + 1}{2q^2 + 2},$$

$$\operatorname{arsinh}(q) = q\sqrt{q^2 + 1} \frac{\chi + 3 - 2\chi q^2}{\chi - 1 + 2q^2(1 + 2\chi)}$$



$$\chi = \frac{V}{\epsilon U}$$

## Structural part of the problem for free elastic plate



Euler's beam equation:

$$\mu \frac{\partial^2}{\partial t^2} \zeta + \theta \frac{\partial^4}{\partial s^4} \zeta = p(s+t, 0, t) - \mu \kappa$$

$$\frac{\partial^2}{\partial s^2} \zeta = \frac{\partial^3}{\partial s^3} \zeta = 0 \quad (s=0, s=1)$$

$h$  plate thickness

$$\mu = \frac{\rho_S h}{\rho_F L} \quad D \text{ flexural rigidity}$$

$$\theta = \frac{D}{\rho_F L^3 U^2} \quad \rho_S \text{ plate density}$$

$$\kappa = \frac{gL}{\varepsilon U^2} \quad \rho_F \text{ fluid density}$$

$$\zeta(s, t) = \sum_{k=0}^{\infty} a_k(t) \psi_k(s)$$

$$\frac{\partial^4}{\partial s^4} \psi_k = \lambda_k^4 \psi_k \quad (0 < s < 1)$$

$$\frac{\partial^2}{\partial s^2} \psi_k = \frac{\partial^3}{\partial s^3} \psi_k = 0 \quad (s=0, s=1)$$

rigid modes of translation and rotation:

$$\psi_0(s), \quad \psi_1(s)$$

normal modes for elastic deflection:

$$\psi_k(s), \quad k \geq 2$$

## Coupling of structural and hydrodynamic part

$$\mu \frac{d^2 a_k}{dt^2} + \theta \lambda_k^4 a_k = \int_t^d p(x, 0, t) \psi_k(x-t) dx - \mu \kappa \delta_{0k}$$

Hydrodynamic pressure:

$$p(x, 0, t) = -\frac{\dot{d} S(t)}{\pi(d-t)} \sqrt{\frac{x-t}{d-x}} - \frac{1}{\pi} \sqrt{(x-t)(d-x)} T(x, t),$$

where

$$S(t) = \int_0^t \sqrt{\frac{t-\xi}{d-\xi}} A(\xi) d\xi + \int_t^d \sqrt{\frac{\xi-t}{d-\xi}} \omega_t(\xi, t) d\xi,$$

$$T(x, t) = \int_t^d \frac{\hat{\omega}_n(\xi, t)}{(\xi-x)\sqrt{(\xi-t)(d-\xi)}} d\xi,$$

$$\hat{\omega}_n(x, t) = \int_t^x \omega_n(\xi, t) d\xi.$$

## Final equations

Euler's beam equation: 
$$\frac{d^2 \vec{a}}{dt^2} = \vec{F} \left( t, d, \vec{a}, \frac{d\vec{a}}{dt}, A(x)|_{x \in (0,t)} \right)$$

Wagner's condition: 
$$\frac{dd}{dt} = G \left( t, d, \vec{a}, \frac{d\vec{a}}{dt}, A(x)|_{x \in (0,t)}, B(x)|_{x \in (0,t)} \right)$$

update of  $A$  and  $B$ : 
$$\int_0^t \sqrt{\frac{d-\xi}{t-\xi}} A(\xi) d\xi = K(t, d, \vec{a}, \frac{d\vec{a}}{dt})$$

$$\int_0^t \sqrt{\frac{d-\xi}{t-\xi}} B(\xi) d\xi = L(t, d, \vec{a}, \frac{d\vec{a}}{dt})$$

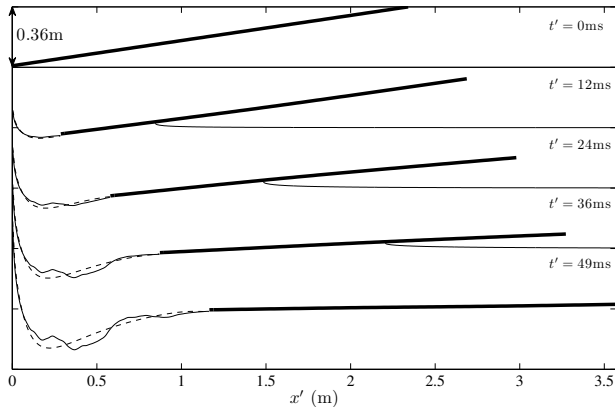
with initial conditions:

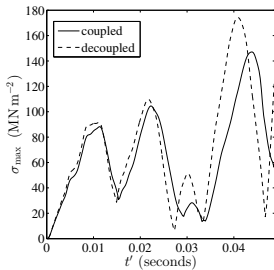
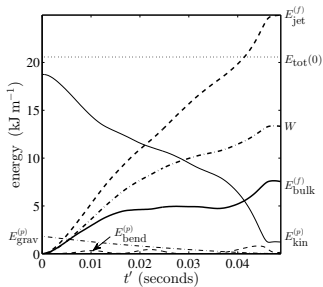
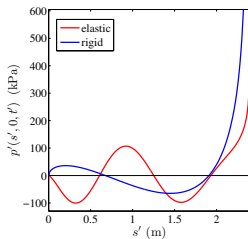
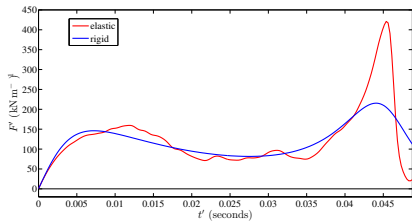
$$\vec{a}(0) = \left( \frac{1}{2}, \frac{1}{6}\sqrt{3}, 0, 0, \dots \right), \quad \frac{d\vec{a}}{dt}(0) = \left( -\frac{v}{\varepsilon U}, 0, 0, \dots \right), \quad d(0) = 0$$

Results for steel plate:

$L = 2.4\text{m}$ ,  $h = 5\text{cm}$ ,  $\varepsilon = 8.6^\circ$ ,  $V = 6\text{ms}^{-1}$ ,  $U = 24\text{ms}^{-1}$

timestep  $\Delta t = 5 \times 10^{-4}$ , 8 elastic modes





## Summary

1. The Wagner model for impact problems of bodies with small deadrise angle into water was introduced.
2. A model for the impact of an elastic plate at high horizontal speed has been presented.
3. Influence of hydroelasticity on the force is significant. Large negative forces appear on the rear part of the plate during impact.

Thank you.

Any questions or comments?



## References



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